

# Top Trumps: materials and alloys

## Gareth Conduit

Patent GB1302743.8 (2013)

Patent GB1307533.8 (2013)

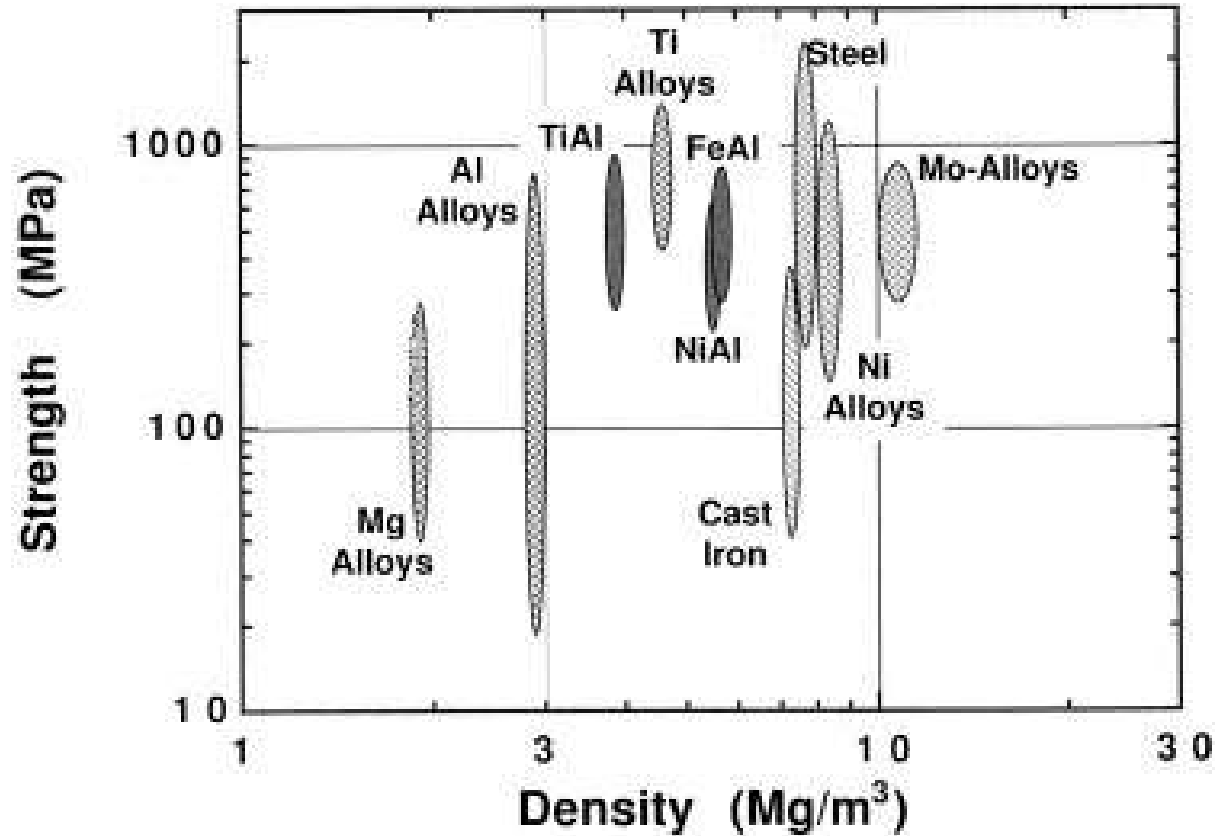
Acta Materialia, **61**, 3378 (2013)

Rolls-Royce Group plc invention submission NC12261 (2012)

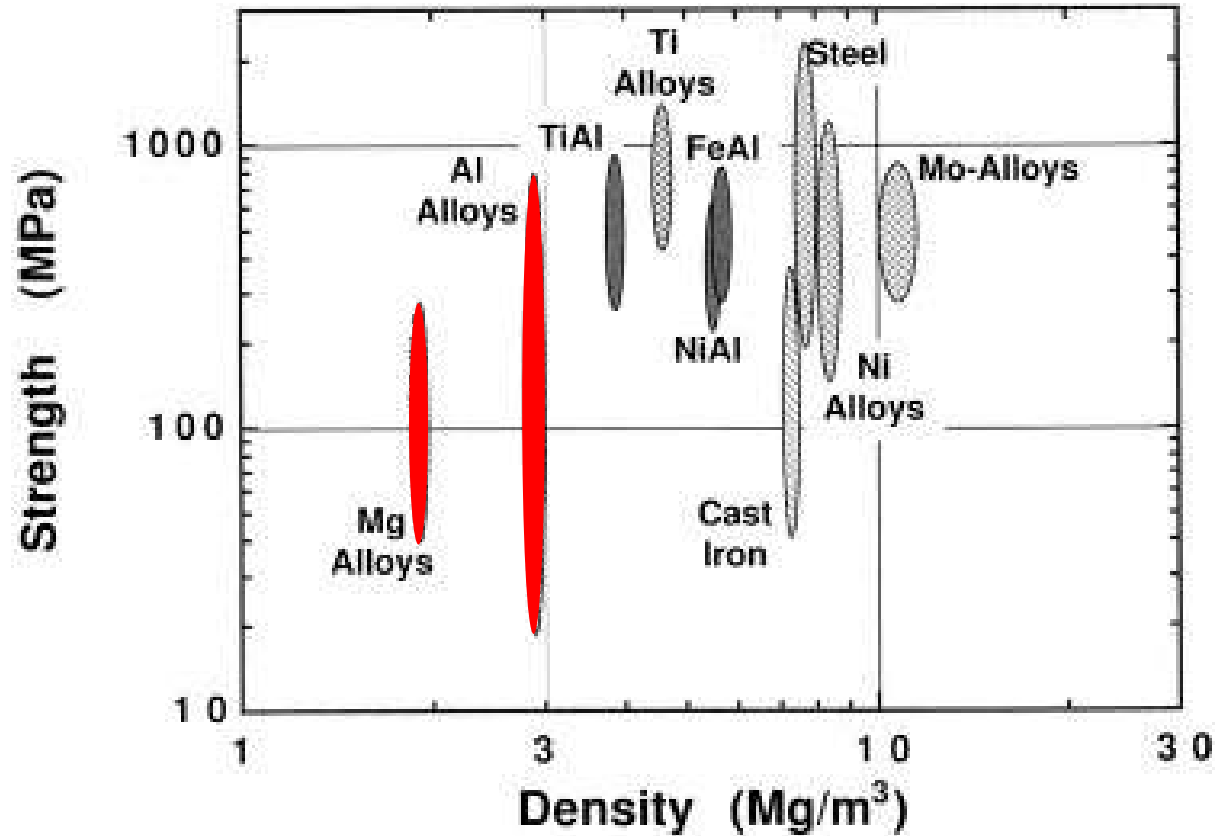
Rolls-Royce Group plc invention submission NC13006 (2013)

Rolls-Royce Group plc invention submission NC13024 (2013)

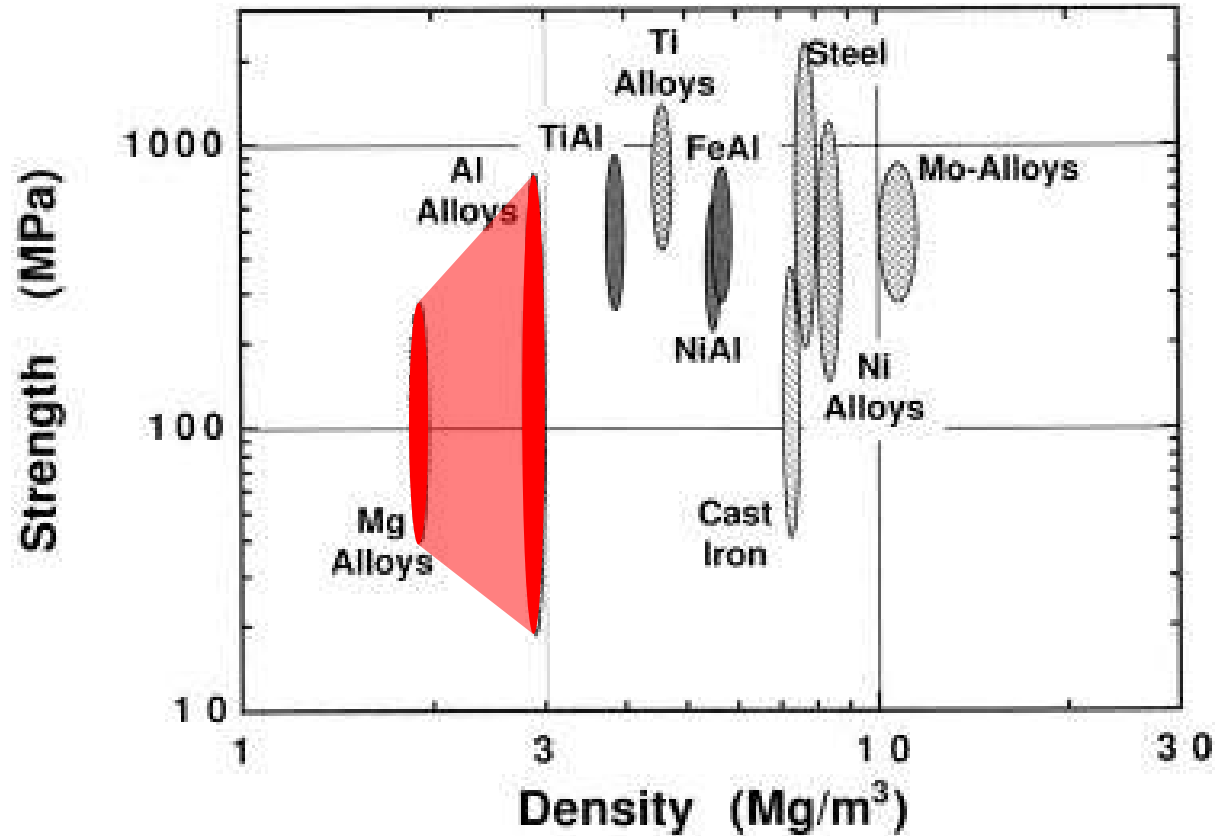
# Materials selection



# Materials selection

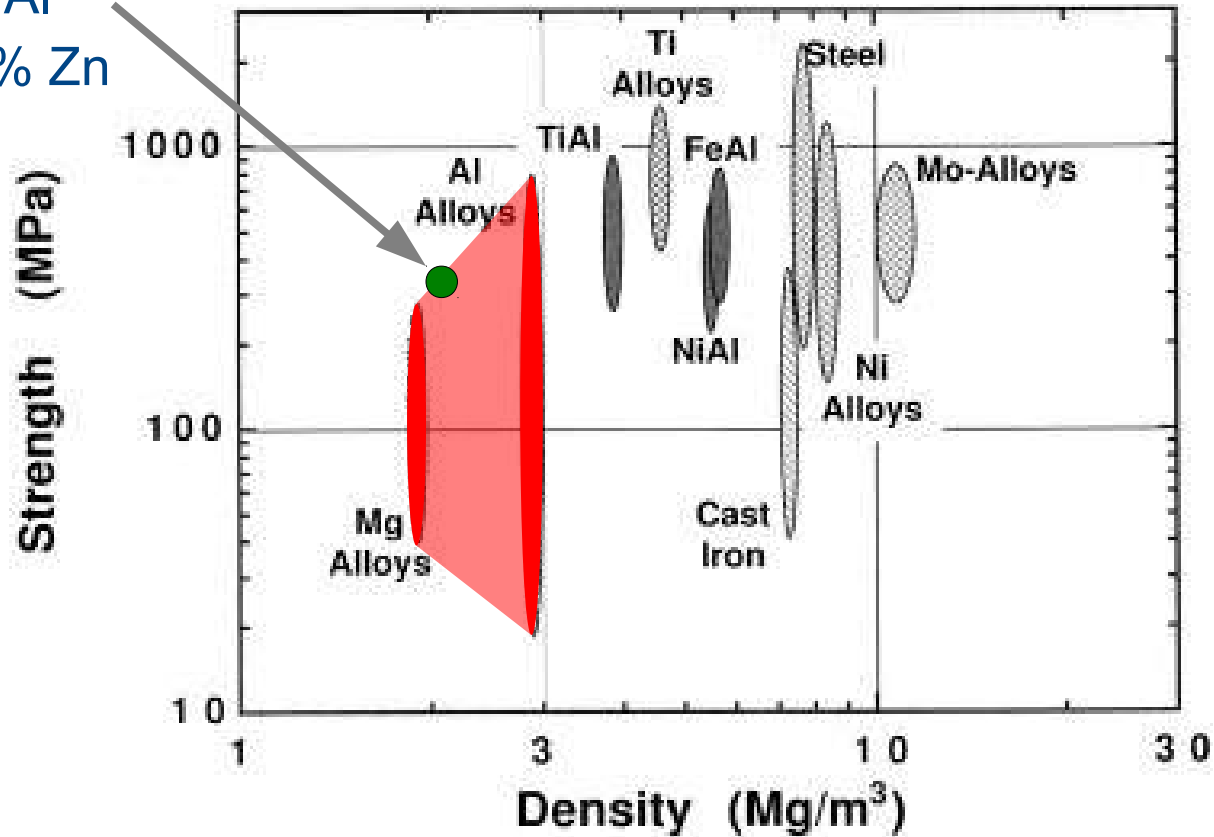


# Materials selection

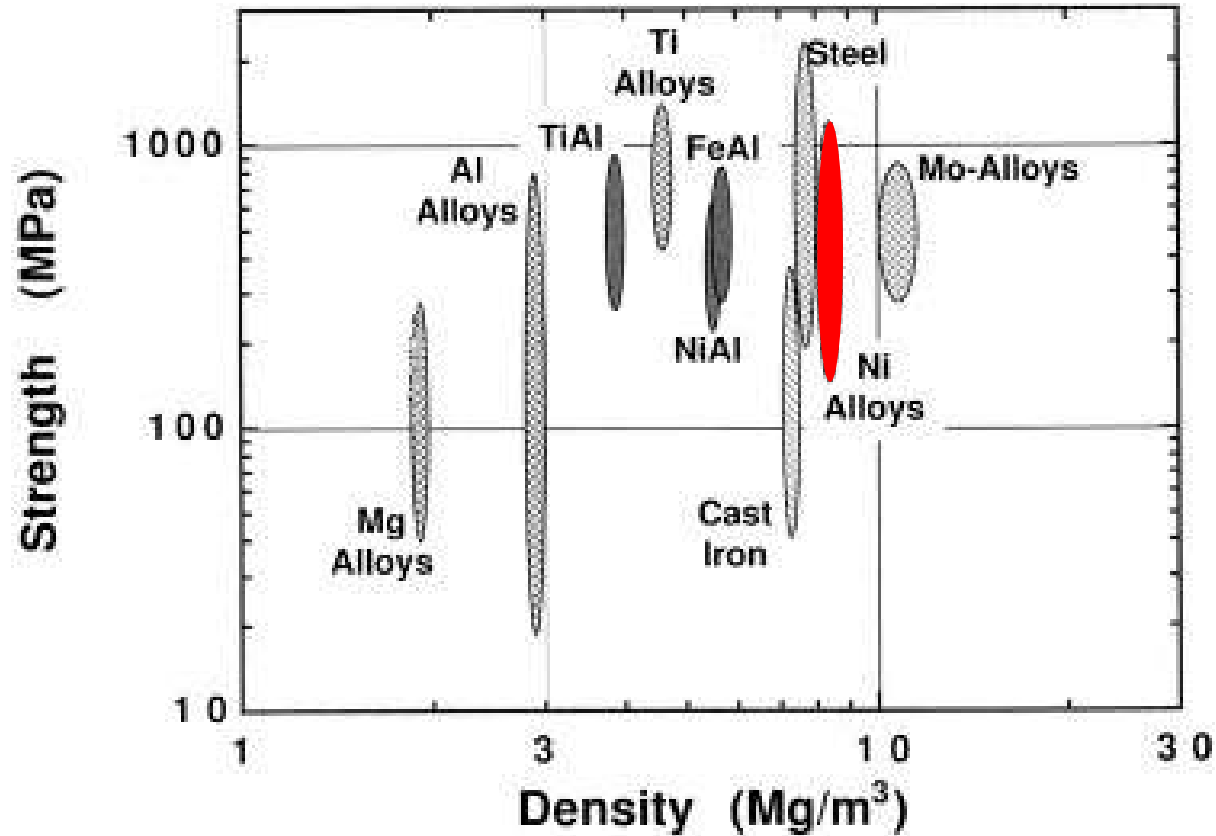


# Materials selection

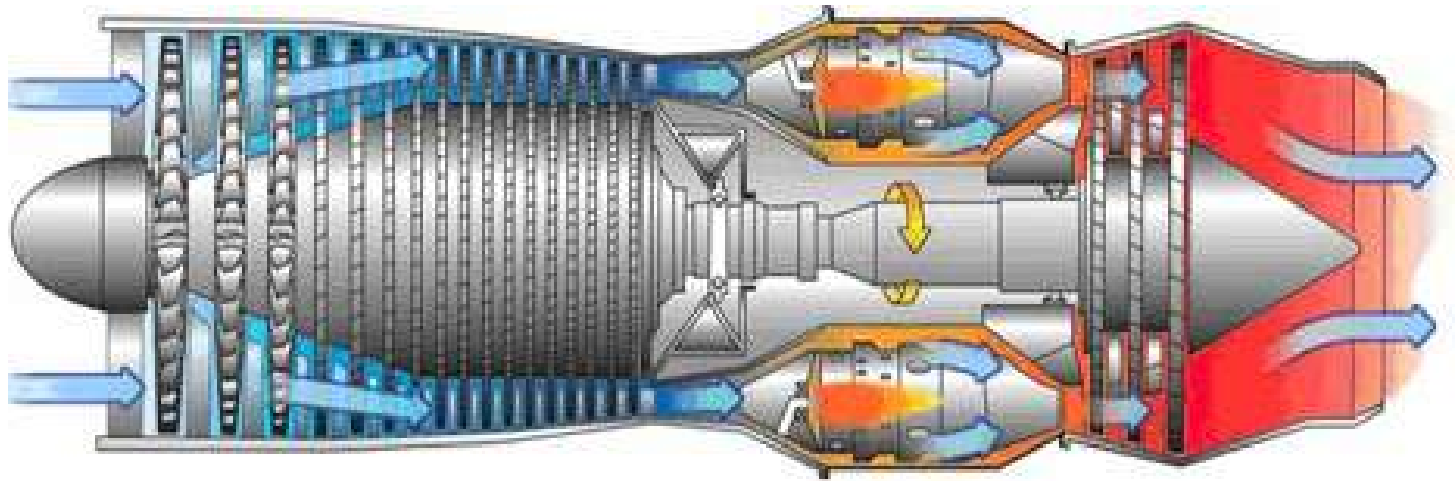
91.5% Mg  
8% Al  
0.5% Zn



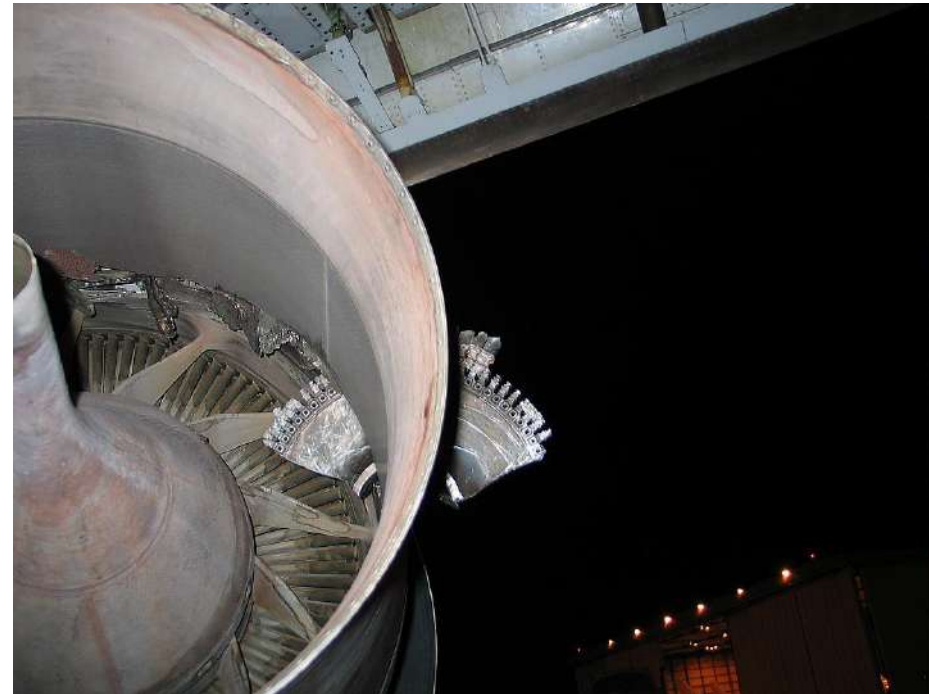
# Materials selection



# Jet engine

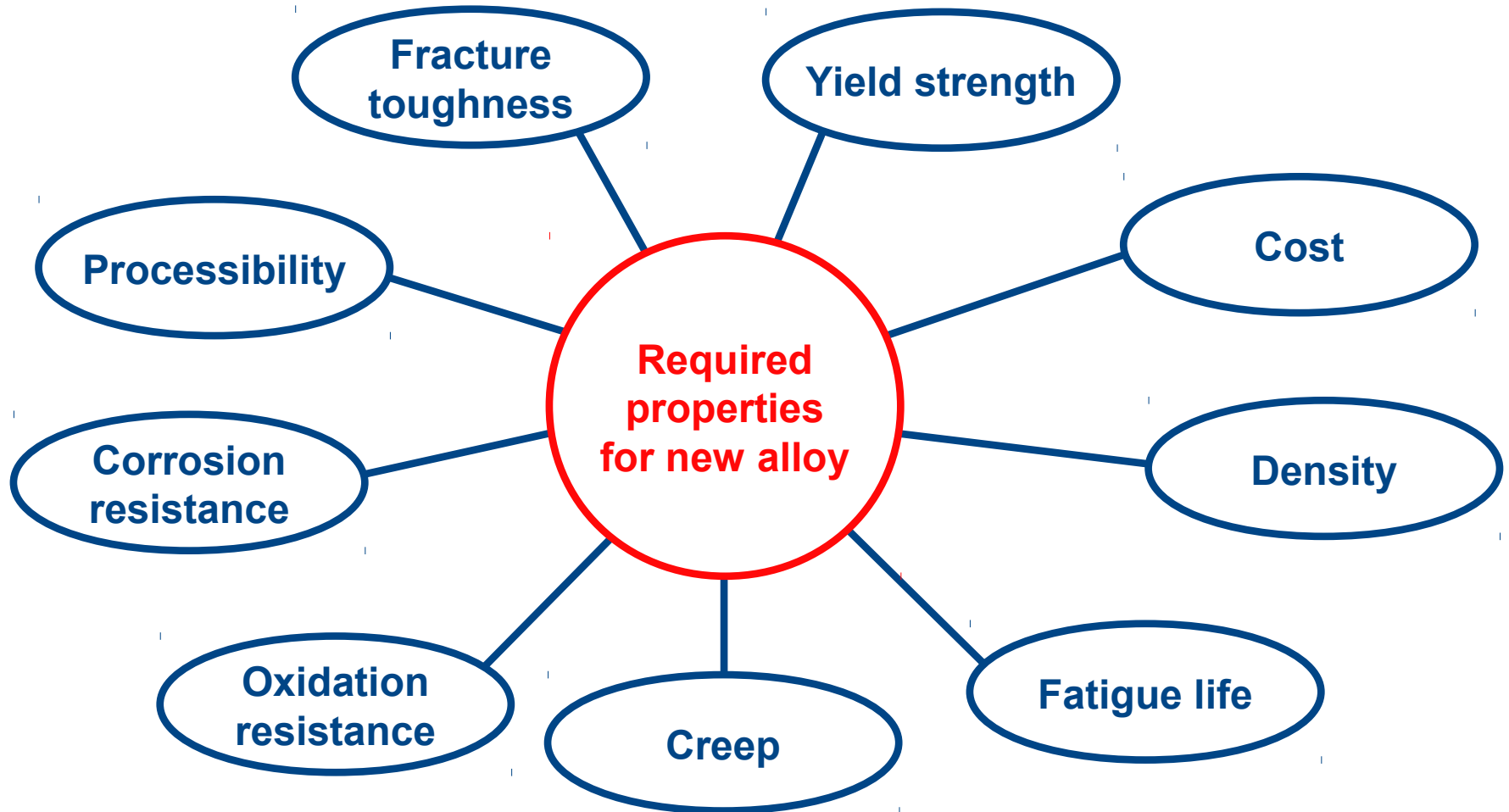


# Jet engine: turbine discs



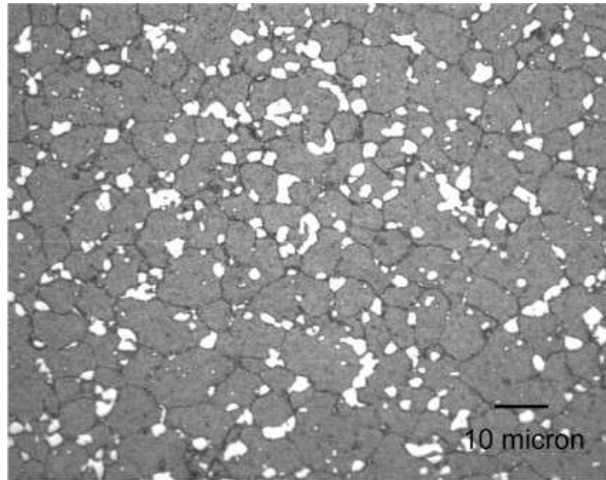


# Designing a new alloy – what is required ?

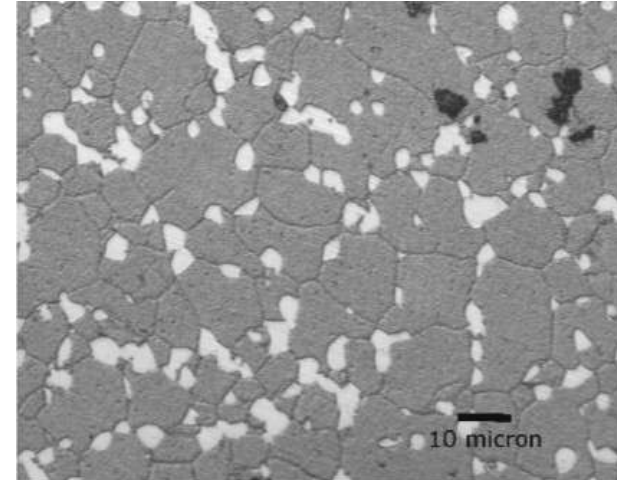


# Contemporary alloys

RR1000

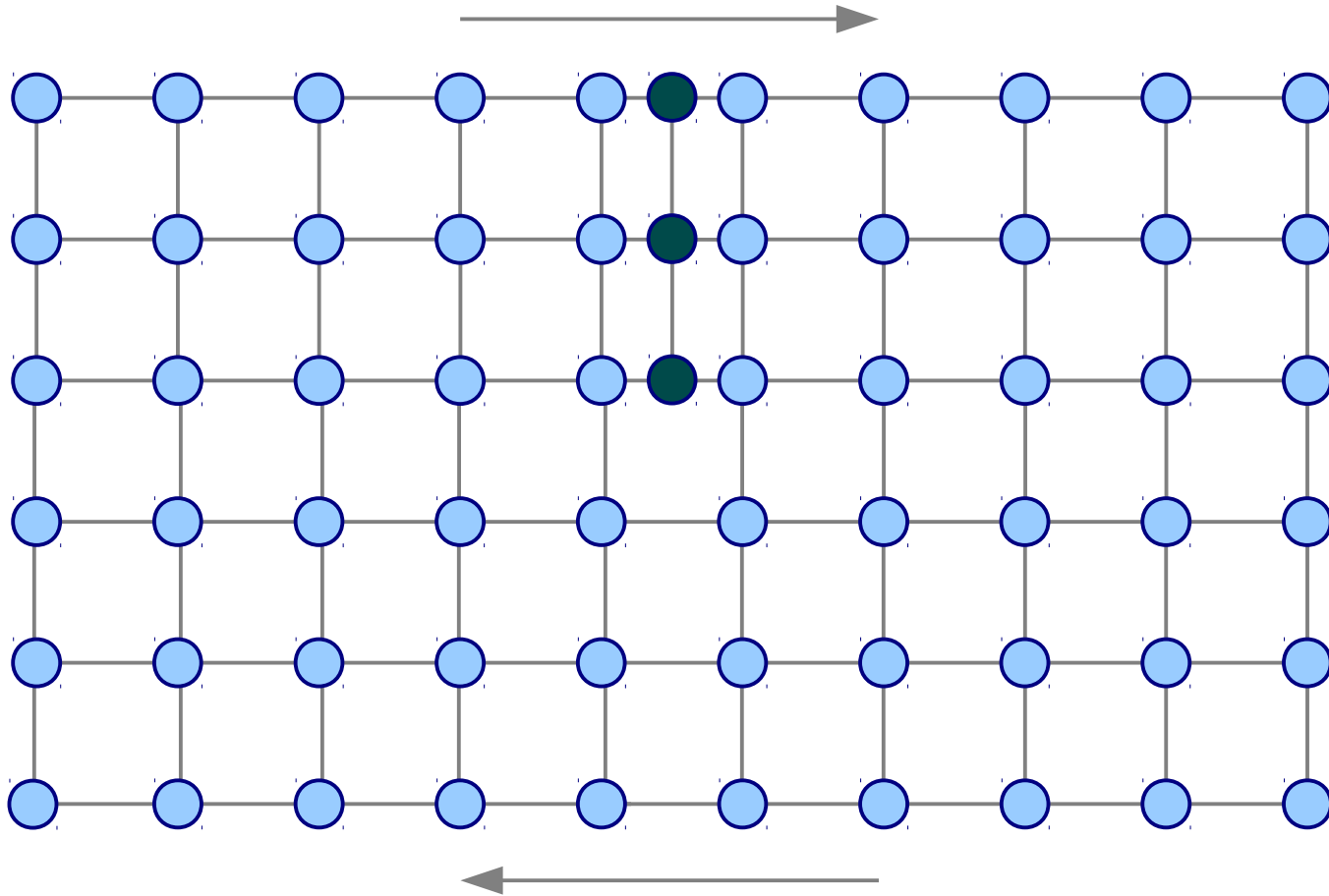


N18

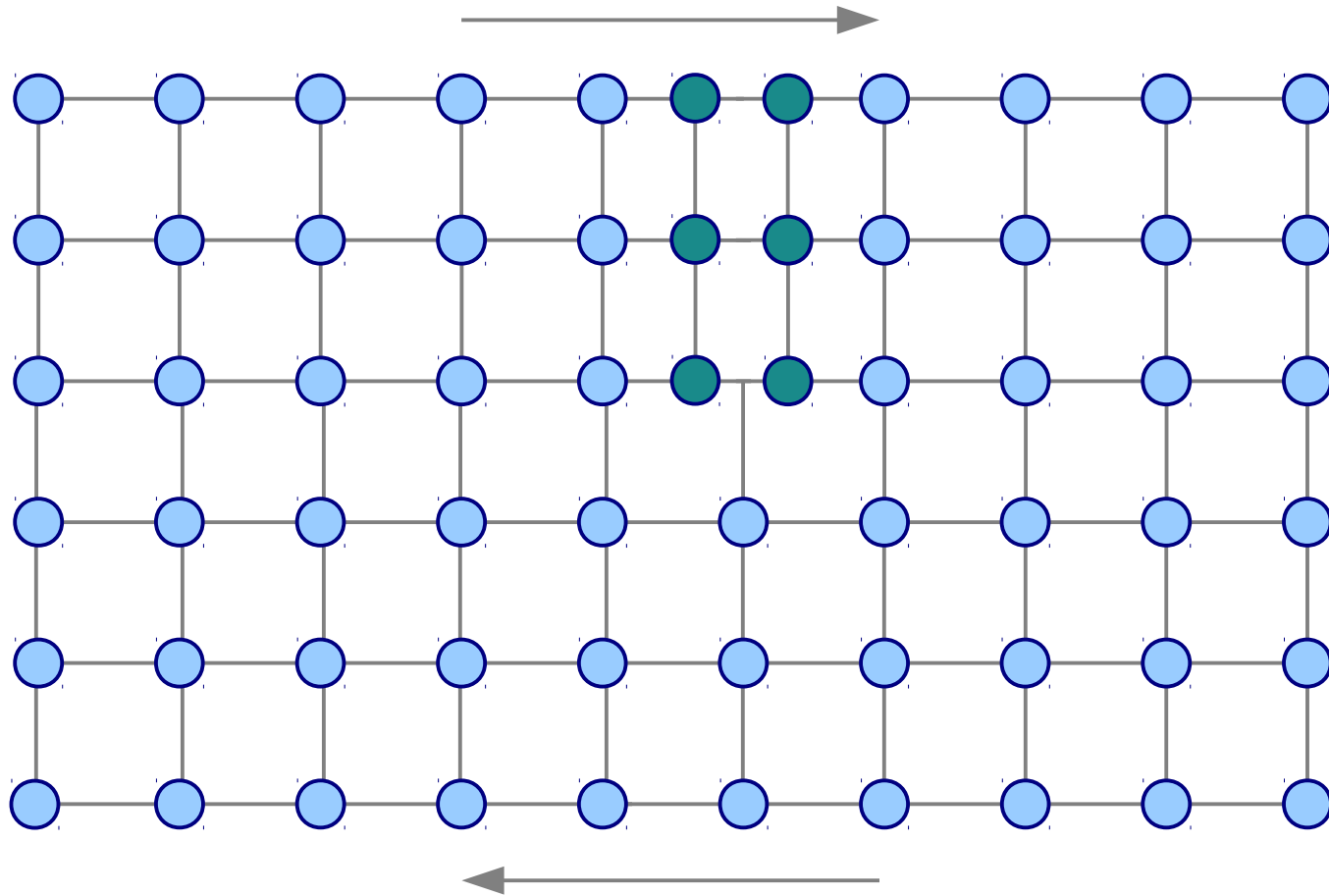


Alloy	Firm	Ni	Cr	Co	Mo	Ti	Al	Ta	Hf	C	W	Nb
RR1000	Rolls Royce	52.4	15	18.5	5	3.6	3	2	0.5	0.03		
N18	SNECMA	58	11.1	15.4	6.4	4.3	4.3		0.5	0.02		
Rene 88	General Elec.	56.5	16	13	4	3.7	2.1			0.03	4	0.7
Waspaloy	UTC	58	19	13	4	3	1.4					

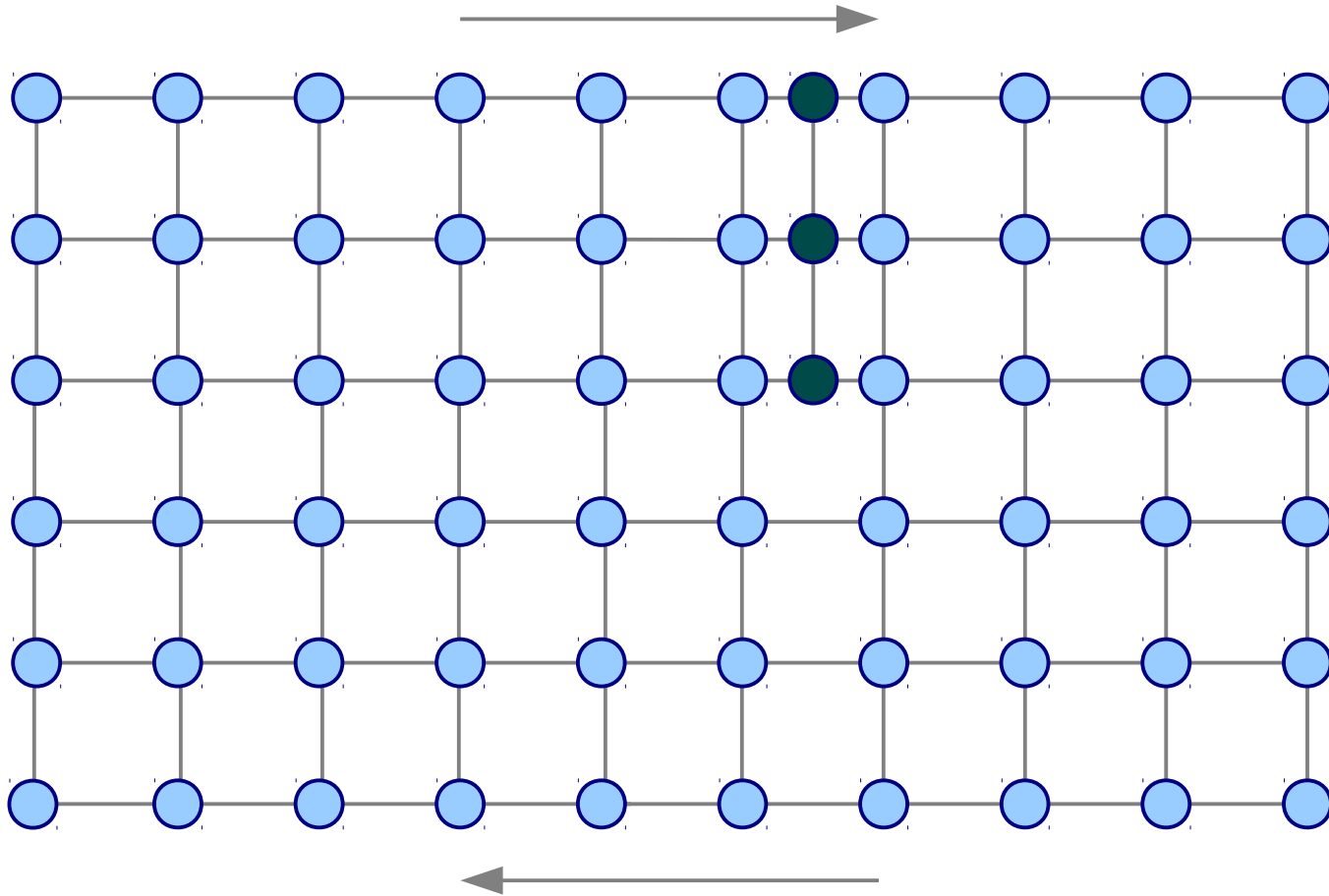
# Creep



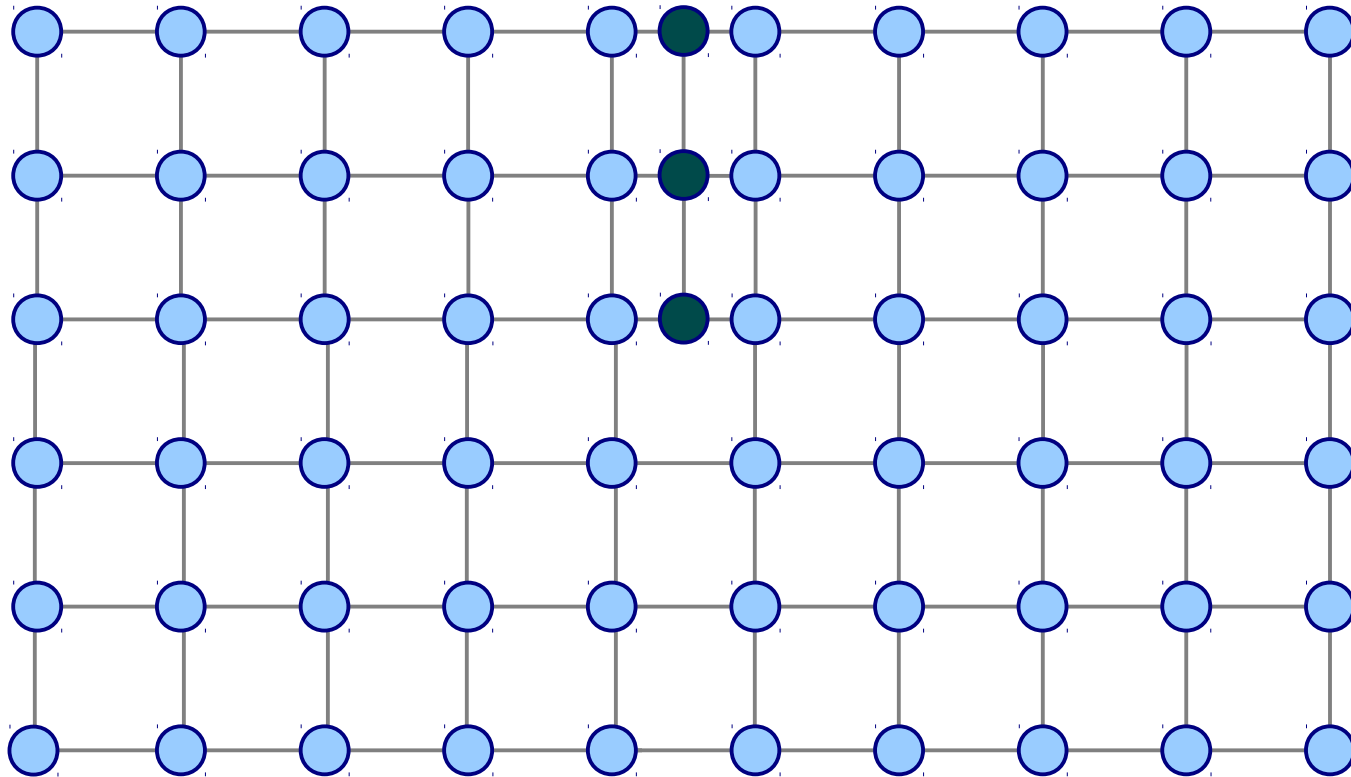
# Creep



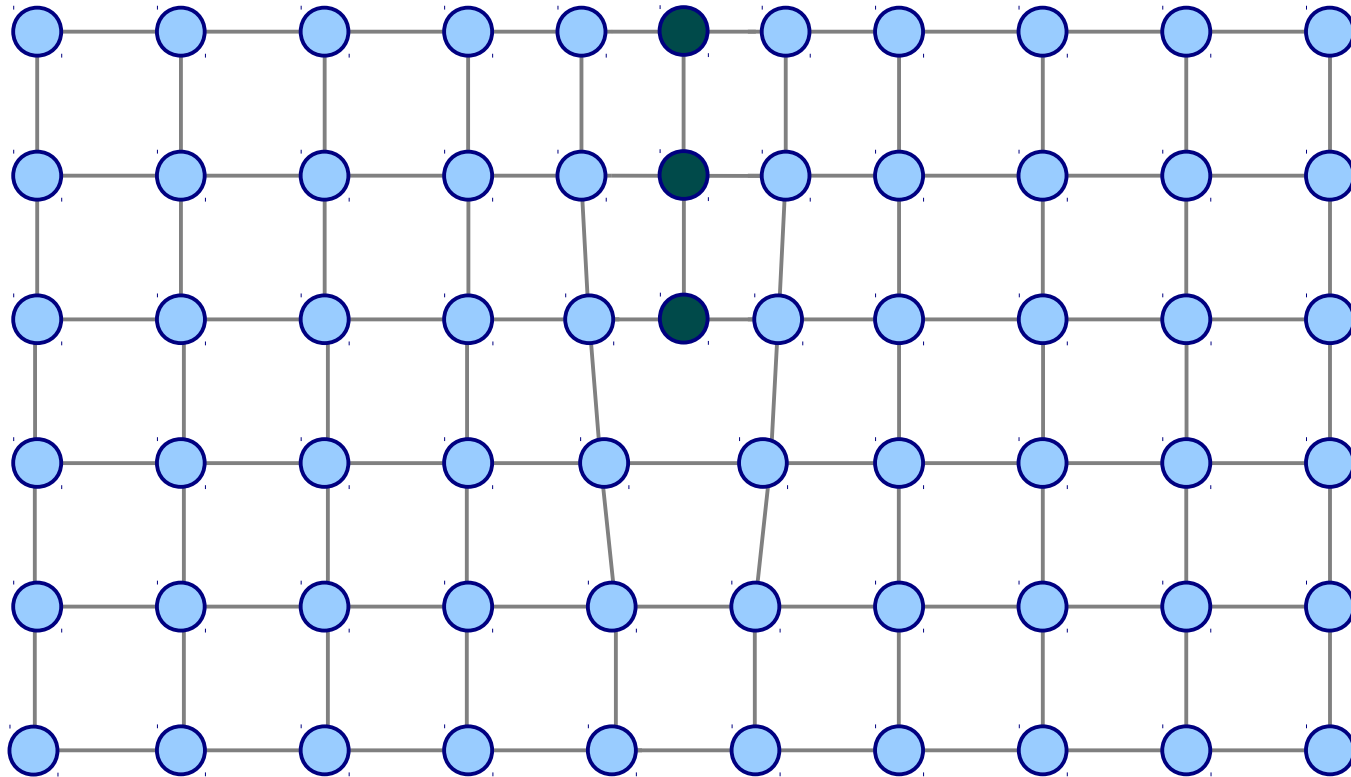
# Creep



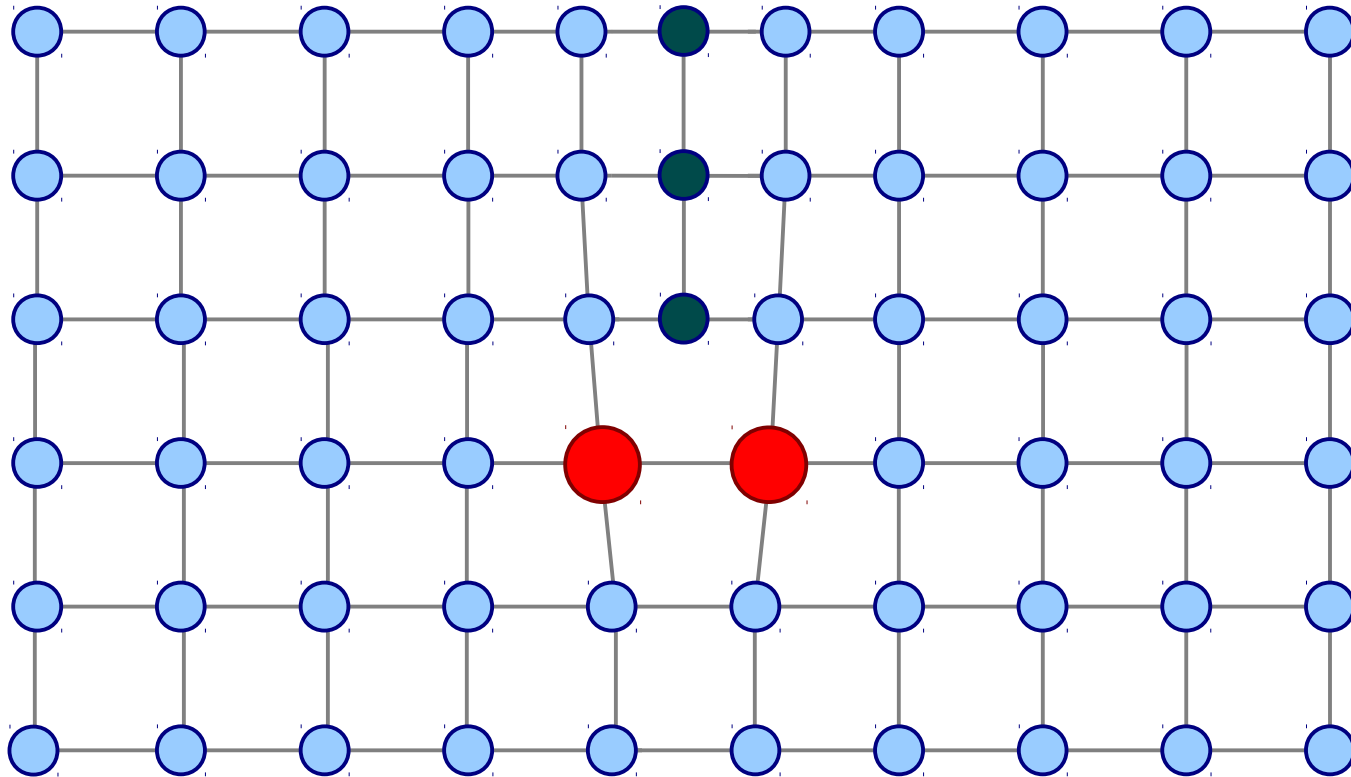
# Solution hardening



# Solution hardening

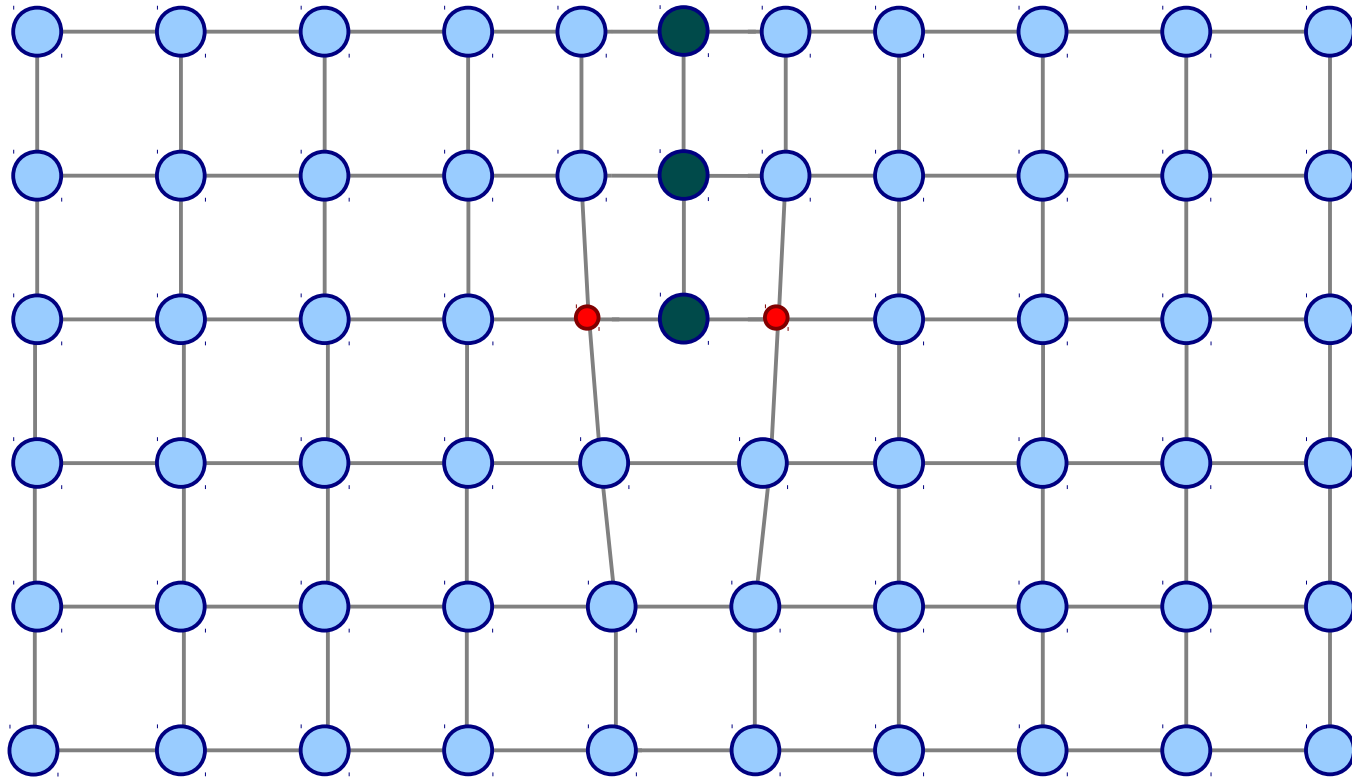


# Solution hardening

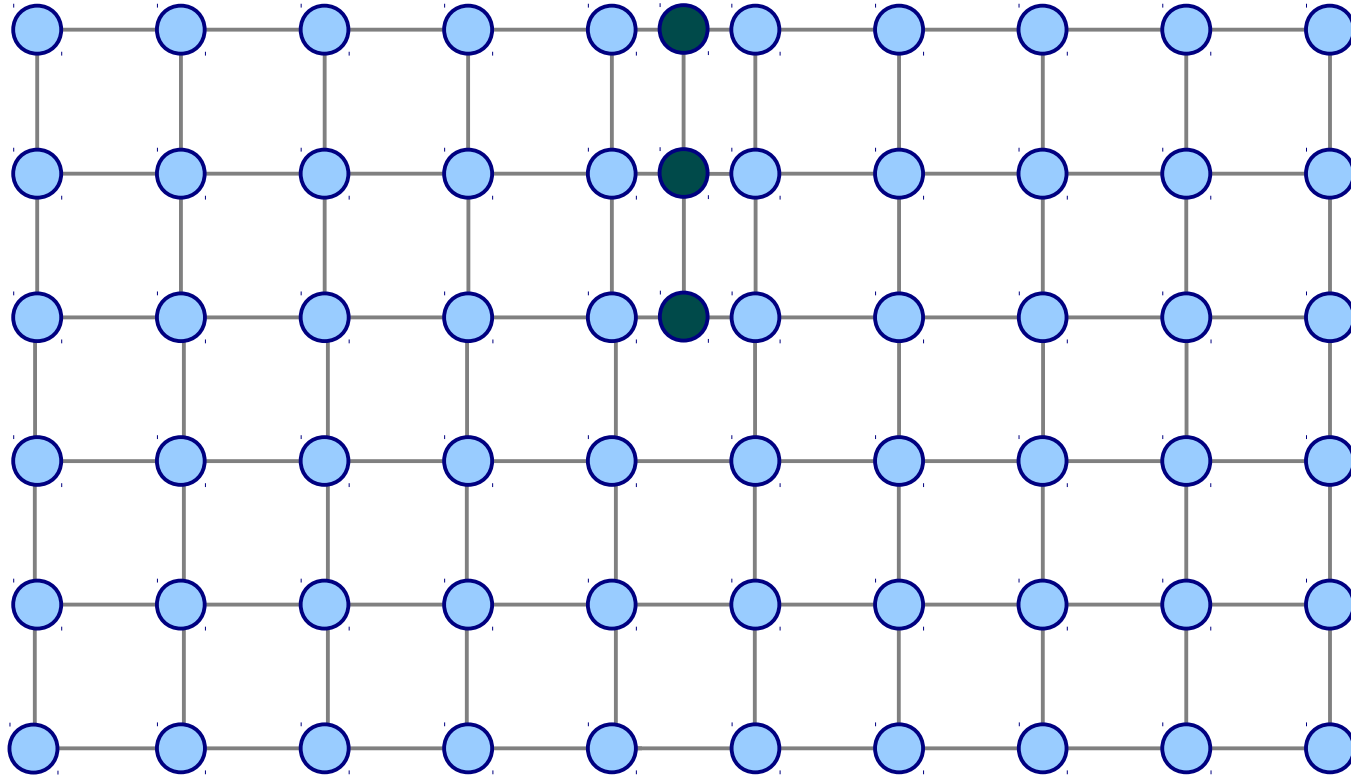




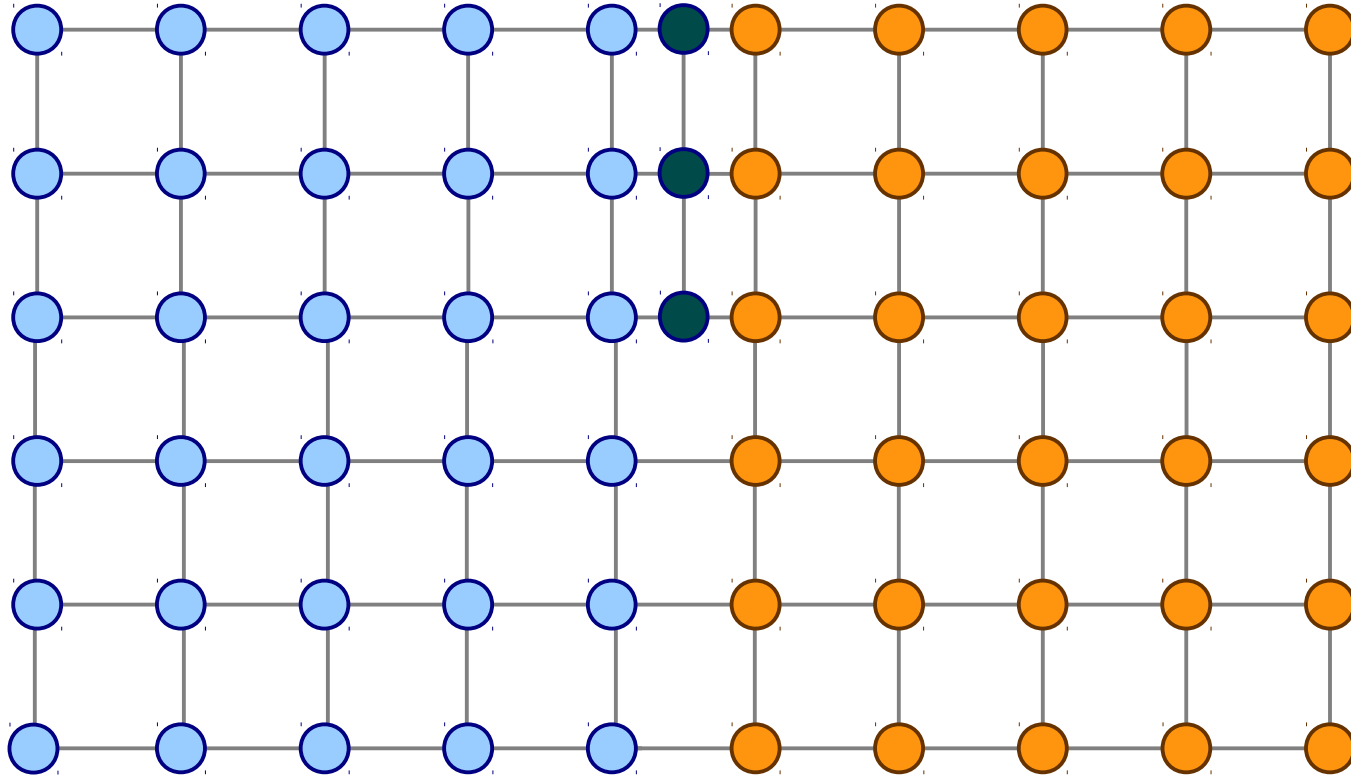
# Solution hardening



# Precipitate hardening

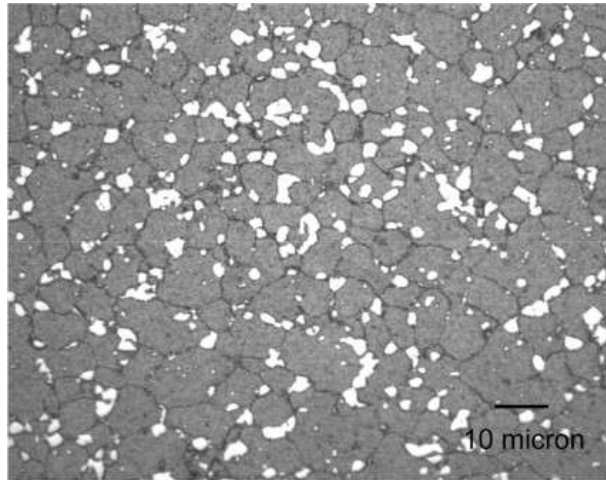


# Precipitate hardening

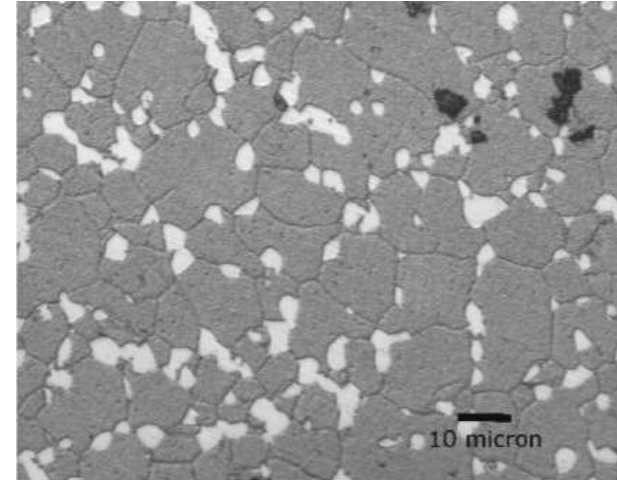


# Contemporary alloys

RR1000



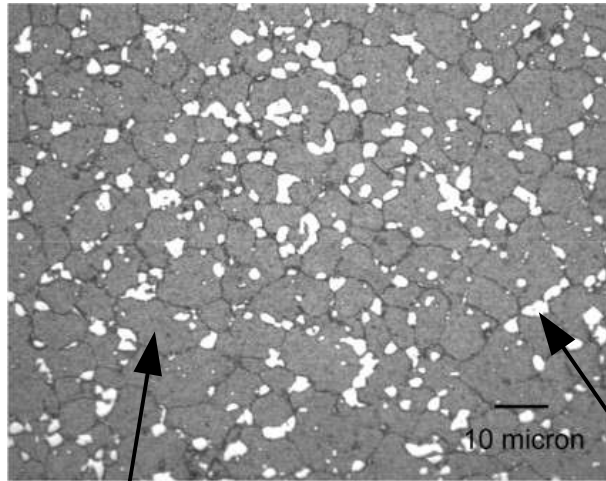
N18



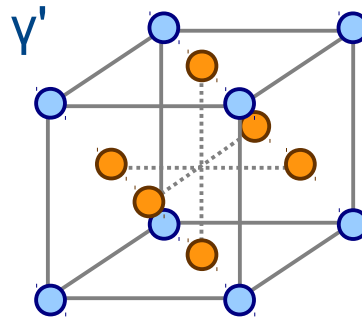
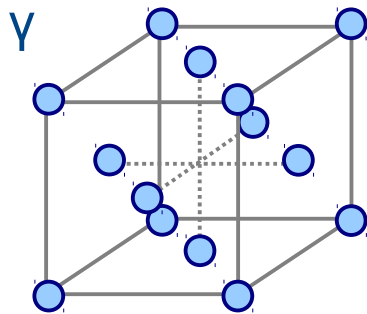
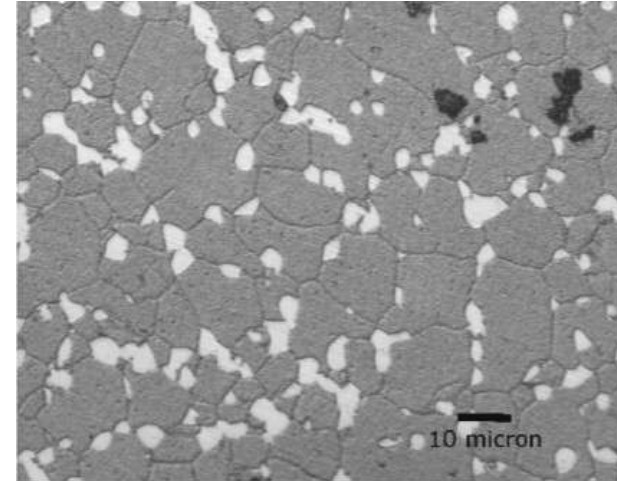
Alloy	Firm	Ni	Cr	Co	Mo	Ti	Al	Ta	Hf	C	W	Nb
RR1000	Rolls Royce	52.4	15	18.5	5	3.6	3	2	0.5	0.03		
N18	SNECMA	58	11.1	15.4	6.4	4.3	4.3		0.5	0.02		
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# Contemporary alloys

RR1000



N18

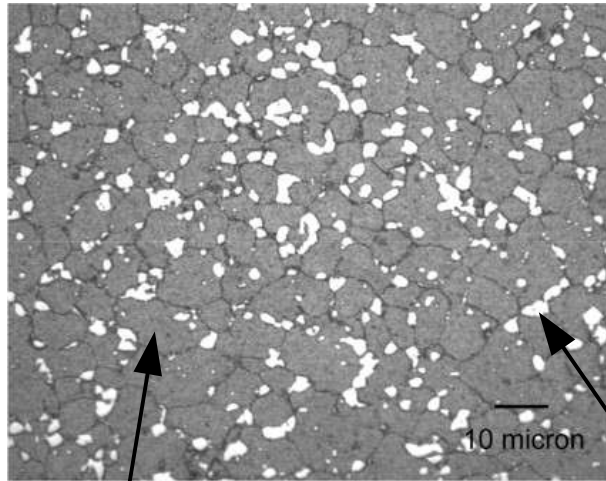


○ Ni

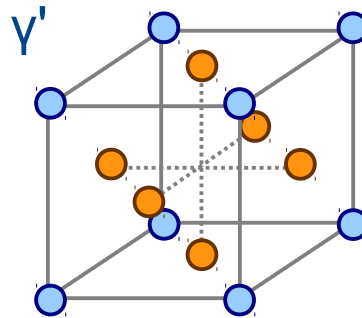
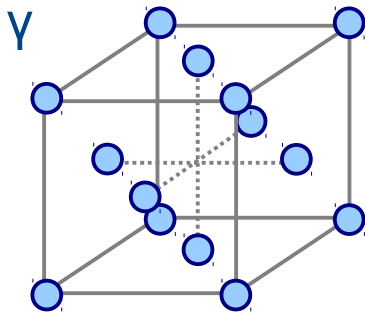
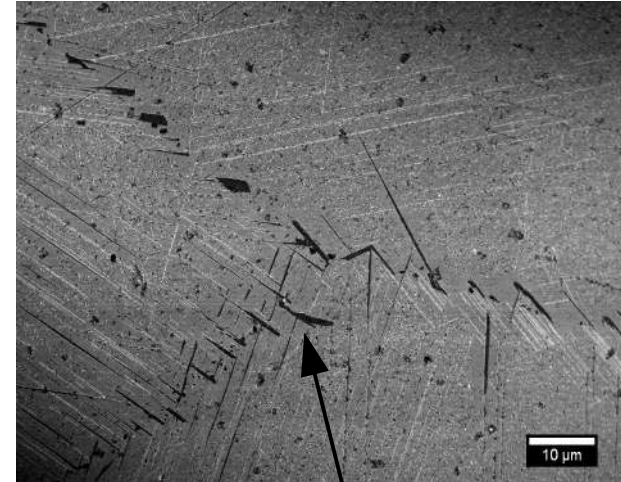
○ Al

# High entropy alloy

RR1000



Attempted alloy



$\eta$  (HCP  $D0_{24}$ )  
 $Ni_3Al$  structure

# Multidimensional design space

**Cr**



**Co**



**Mo**



**W**



**Ta**



**Nb**



**Al**



**Ti**



**Fe**



**Mn**



**Si**



**C**



**B**



**Zr**



**Cu**



**N**



**P**



**V**



**Hf**



**Mg**



**Ni**



**Heat treatment**



# Properties

**Cost \$lb<sup>-1</sup>**

**γ' fraction**

**Stability**

**Density gcm<sup>-3</sup>**

**Yield stress MPa**

**UTS MPa**

**Oxidation index**

**Stress rupture MPa**

**Resistivity μΩcm**

**Entropy Jmol<sup>-1</sup>K<sup>-1</sup>**



# Properties

Cost \$lb<sup>-1</sup>

γ' fraction

Stability

Density gcm<sup>-3</sup>

Yield stress MPa

UTS MPa

Oxidation index

Stress rupture MPa

Resistivity μΩcm

Entropy Jmol<sup>-1</sup>K<sup>-1</sup>

$$\text{Cost}[\$/\text{lb}] = 9.59n_{\text{Ni}} + 0.94n_{\text{Al}} + 6.77n_{\text{Cr}} \\ + 16.5n_{\text{Co}} + 19.6n_{\text{Mo}} + 5.44n_{\text{Ti}}$$

# Properties

Collect data for yield stress from 2248 alloys

Cost  $\text{\$lb}^{-1}$

$\gamma'$  fraction

Stability

Density  $\text{gcm}^{-3}$

**Yield stress MPa**

UTS MPa

Oxidation index

Stress rupture MPa

Resistivity  $\mu\Omega\text{cm}$

Entropy  $\text{Jmol}^{-1}\text{K}^{-1}$

# Properties

Cost \$lb<sup>-1</sup>  
γ' fraction  
Stability  
Density gcm<sup>-3</sup>  
**Yield stress MPa**  
UTS MPa  
Oxidation index  
Stress rupture MPa  
Resistivity μΩcm  
Entropy Jmol<sup>-1</sup>K<sup>-1</sup>

Collect data for yield stress from 2248 alloys



Generate neural network model

$$\text{YS}[\text{MPa}] = F(n_{\text{Ni}}, n_{\text{Al}}, n_{\text{Cr}}, n_{\text{Co}}, n_{\text{Mo}}, n_{\text{Ti}}, T_{\text{HT}}, t_{\text{HT}})$$

# Properties

Cost \$lb<sup>-1</sup>  
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**Yield stress MPa**  
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Calculate uncertainty in neural network model

# Properties

Cost \$lb<sup>-1</sup>  
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Density gcm<sup>-3</sup>  
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# Properties

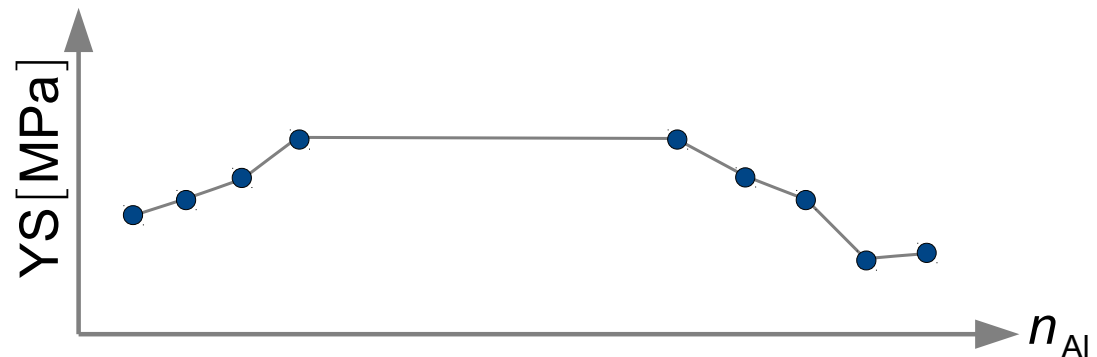
Cost  $\$/\text{lb}^{-1}$   
 $\gamma'$  fraction  
Stability  
Density  $\text{gcm}^{-3}$   
Yield stress MPa  
UTS MPa  
Oxidation index  
Stress rupture MPa  
Resistivity  $\mu\Omega\text{cm}$   
Entropy  $\text{Jmol}^{-1}\text{K}^{-1}$

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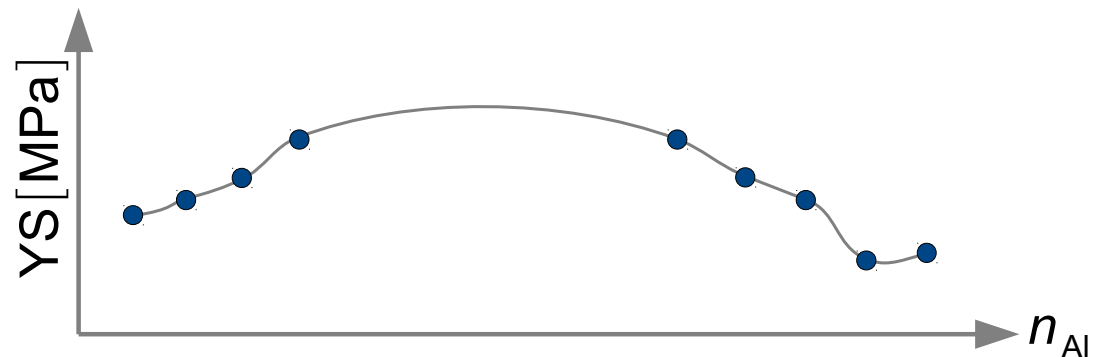
Cost \$lb<sup>-1</sup>  
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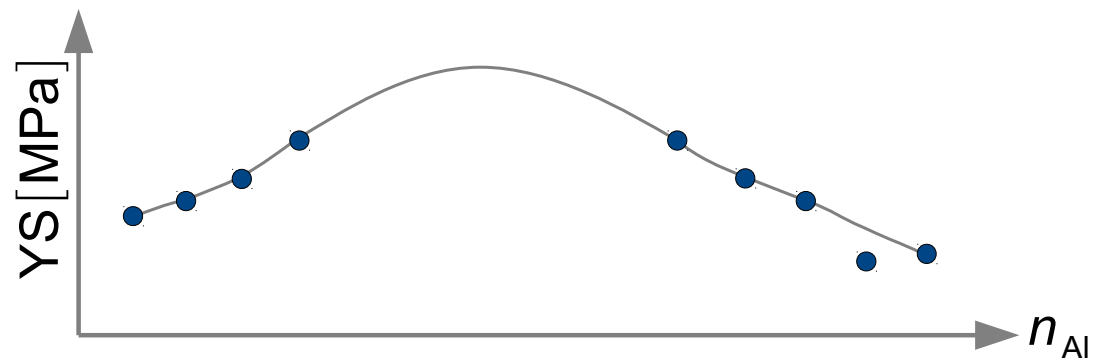
Cost \$lb<sup>-1</sup>  
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# Properties

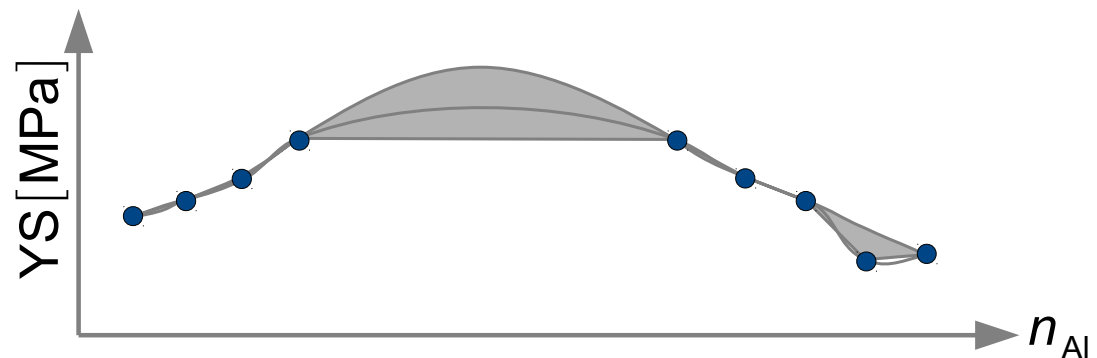
Cost \$lb<sup>-1</sup>  
γ' fraction  
Stability  
Density gcm<sup>-3</sup>  
**Yield stress MPa**  
UTS MPa  
Oxidation index  
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Generate neural network model

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Calculate uncertainty in neural network model



# Properties

Cost \$lb<sup>-1</sup>

$\gamma'$  fraction

Stability

Density gcm<sup>-3</sup>

Yield stress MPa

UTS MPa

Oxidation index

Stress rupture MPa

Resistivity  $\mu\Omega\text{cm}$

Entropy Jmol<sup>-1</sup>K<sup>-1</sup>

Calculate grid of

$$F_{(\gamma, \gamma')} (n_{\text{Ni}}, n_{\text{Al}}, n_{\text{Cr}}, n_{\text{Co}}, n_{\text{Mo}}, n_{\text{Ti}})$$

# Properties

Cost \$lb<sup>-1</sup>  
**γ' fraction**  
Stability  
Density gcm<sup>-3</sup>  
Yield stress MPa  
UTS MPa  
Oxidation index  
Stress rupture MPa  
Resistivity μΩcm  
Entropy Jmol<sup>-1</sup>K<sup>-1</sup>

Calculate grid of

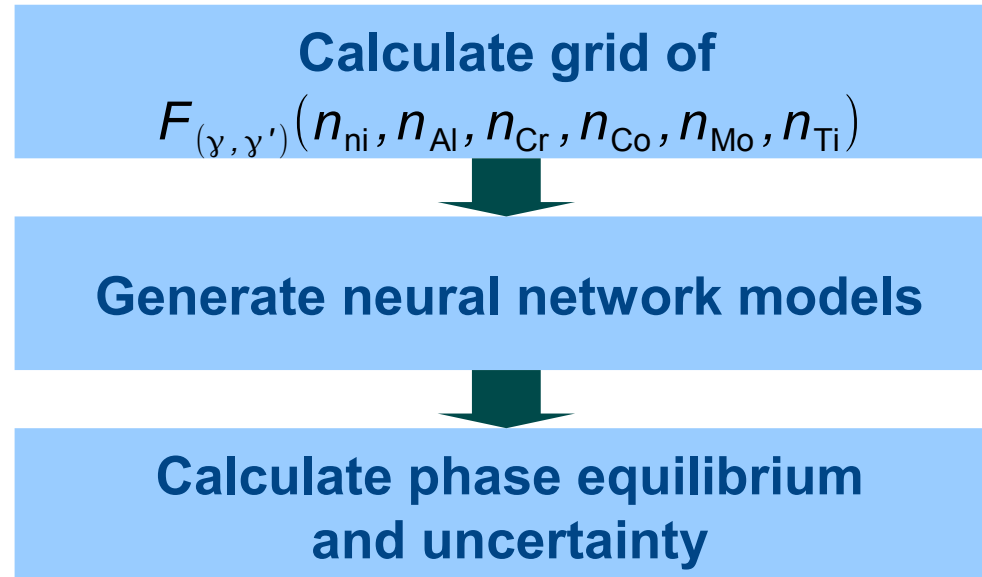
$$F_{(\gamma, \gamma')} (n_{\text{Ni}}, n_{\text{Al}}, n_{\text{Cr}}, n_{\text{Co}}, n_{\text{Mo}}, n_{\text{Ti}})$$



Generate neural network models

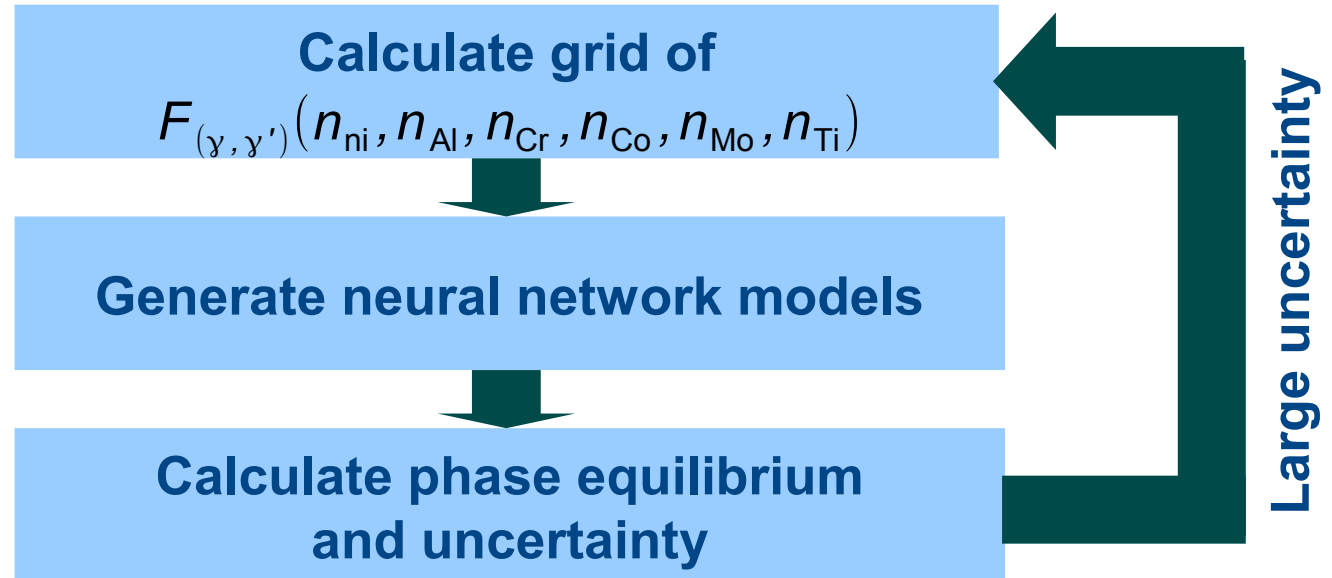
# Properties

Cost \$lb<sup>-1</sup>  
 $\gamma'$  fraction  
Stability  
Density gcm<sup>-3</sup>  
Yield stress MPa  
UTS MPa  
Oxidation index  
Stress rupture MPa  
Resistivity  $\mu\Omega\text{cm}$   
Entropy Jmol<sup>-1</sup>K<sup>-1</sup>



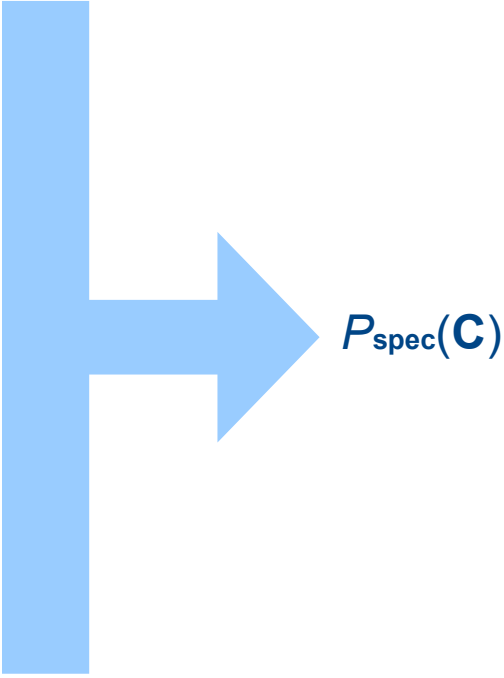
# Properties

Cost \$lb<sup>-1</sup>  
 $\gamma'$  fraction  
Stability  
Density gcm<sup>-3</sup>  
Yield stress MPa  
UTS MPa  
Oxidation index  
Stress rupture MPa  
Resistivity  $\mu\Omega\text{cm}$   
Entropy Jmol<sup>-1</sup>K<sup>-1</sup>



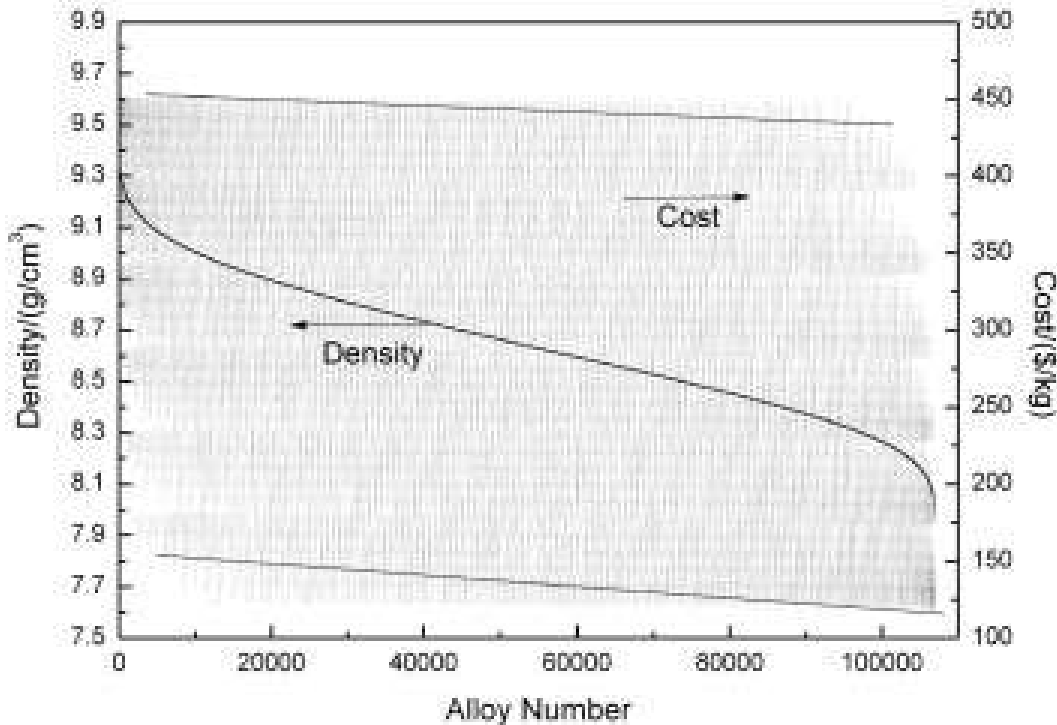
# Merit factor

<b>Cost \$lb<sup>-1</sup></b>	$S_{\text{cost}}$	$P_{\text{cost}}(\mathbf{C})$
<b><math>\gamma'</math> fraction</b>	$S_{\gamma'}$	$P_{\gamma'}(\mathbf{C})$
<b>Stability</b>	$S_{\text{stable}}$	$P_{\text{stable}}(\mathbf{C})$
<b>Density gcm<sup>-3</sup></b>	$S_{\text{density}}$	$P_{\text{density}}(\mathbf{C})$
<b>Yield stress MPa</b>	$S_{\text{YS}}$	$P_{\text{YS}}(\mathbf{C})$
<b>UTS MPa</b>	$S_{\text{UTS}}$	$P_{\text{UTS}}(\mathbf{C})$
<b>Oxidation index</b>	$S_{\text{oxidize}}$	$P_{\text{oxidize}}(\mathbf{C})$
<b>Stress rupture MPa</b>	$S_{\text{SR}}$	$P_{\text{SR}}(\mathbf{C})$
<b>Resistivity <math>\mu\Omega\text{cm}</math></b>	$S_{\text{resis}}$	$P_{\text{resis}}(\mathbf{C})$
<b>Entropy Jmol<sup>-1</sup>K<sup>-1</sup></b>	$S_{\text{entropy}}$	$P_{\text{entropy}}(\mathbf{C})$



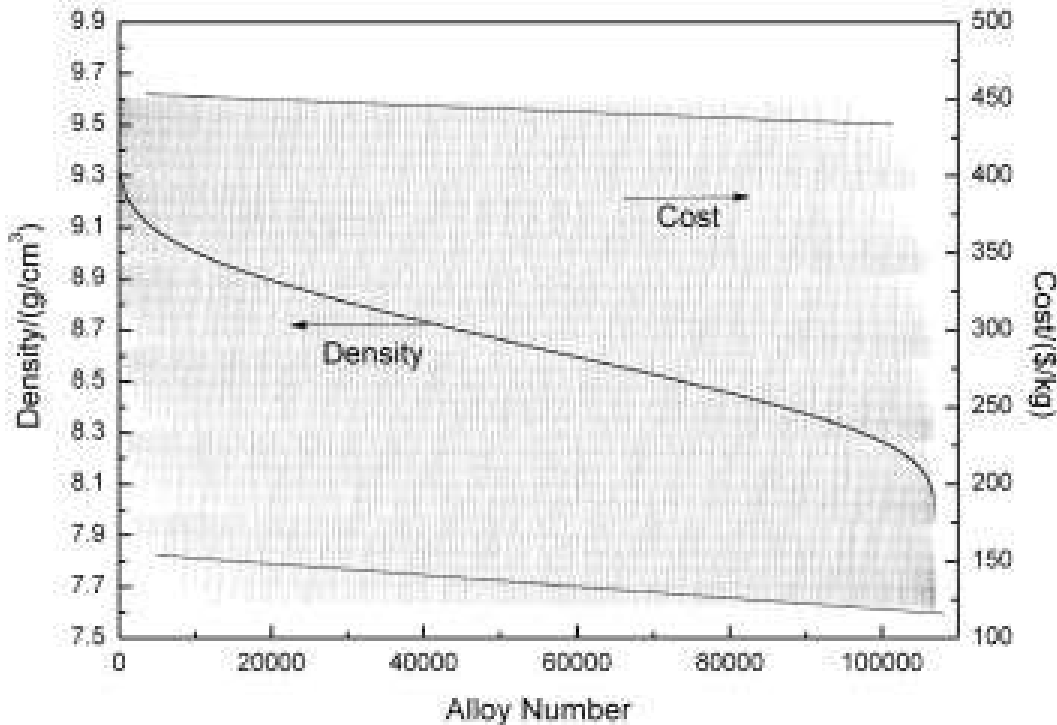
$P_{\text{spec}}(\mathbf{C})$

# Optimization – tradeoff diagrams



R.C. Reed, T. Tao, & N. Warnken, *Acta Materialia* **57**, 5898 (2009)

# Optimization – tradeoff diagrams

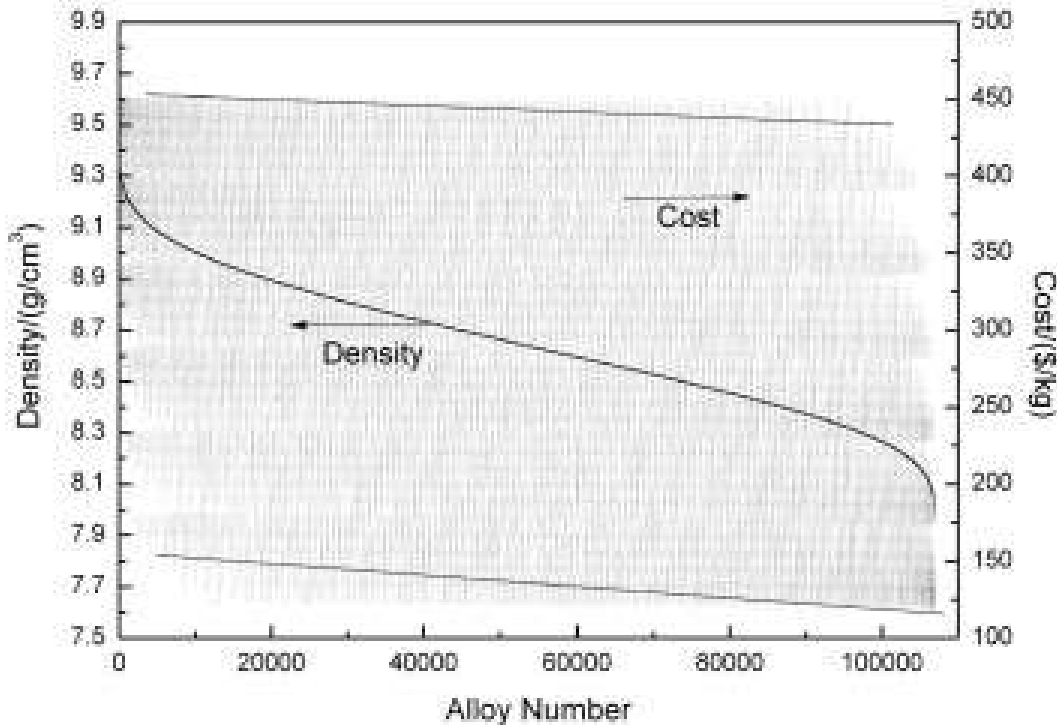


**Probability of success**  
 $0.5^5 \sim 0.03$

R.C. Reed, T. Tao, & N. Warnken, *Acta Materialia* **57**, 5898 (2009)



# Optimization – tradeoff diagrams



**Probability of success**

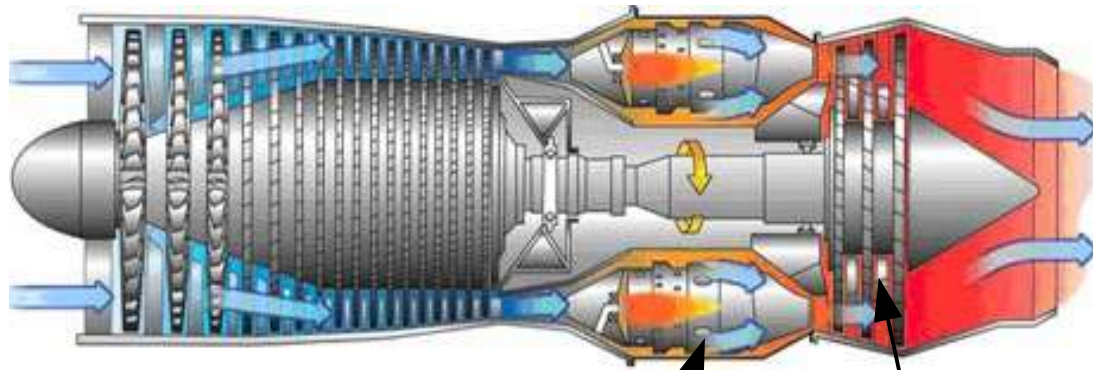
$0.5^5 \sim 0.03$

**Composition resolution**

$100000^{1/6} \sim 7$

R.C. Reed, T. Tao, & N. Warnken, *Acta Materialia* **57**, 5898 (2009)

# Predicted alloys



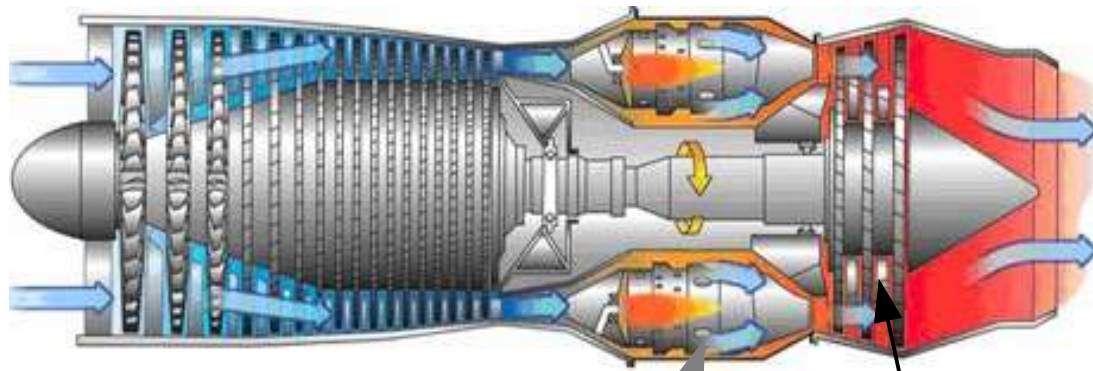
Combustor  
liner

2x disc  
alloy



2x forging  
hammer

# Predicted alloys



Combustor  
liner

**2x disc  
alloy**



2x forging  
hammer

# Case study: RR1000

<b>At 725°C</b>	<b>RR1000</b>
<b>Cost \$lb<sup>-1</sup></b>	13.46 ± 0.01
<b>γ' fraction</b>	42.2 ± 0.9
<b>Stability</b>	89.1 ± 1.6
<b>Density gcm<sup>-3</sup></b>	8.32 ± 0.01
<b>Yield stress MPa</b>	753.4 ± 30.7
<b>UTS MPa</b>	1054.5 ± 24.1
<b>Oxidation index</b>	16.50 ± 0.01
<b>Stress rupture MPa</b>	599.4 ± 18.8
<b>Resistivity μΩcm</b>	9.02 ± 0.01
<b>Entropy Jmol<sup>-1</sup>K<sup>-1</sup></b>	11.60 ± 0.01

	Ni	Cr	Co	Mo	Ti	Al	Ta	Hf	C	W	Mn	B	Ta	Si	Zr	Nb	Fe	T	t
RR1000	52	15	19	5	3.6	3	2	0.5	0.1									800	8

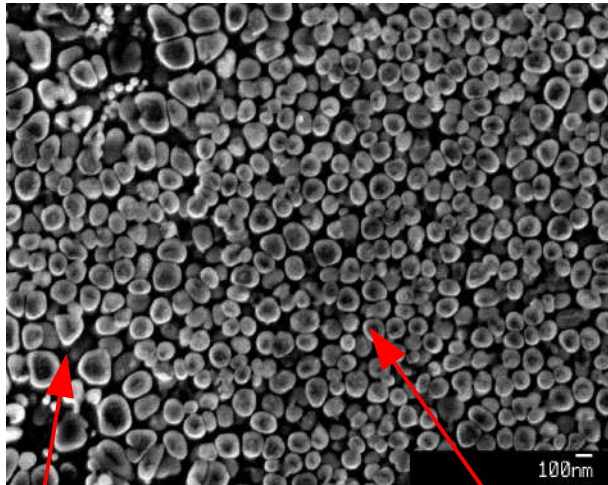
# Case study: improved

At 725°C	RR1000	Optimal
Cost \$lb <sup>-1</sup>	13.46 ± 0.01	11.67 ± 0.01
γ' fraction	42.2 ± 0.9	39.7 ± 3.1
Stability	89.1 ± 1.6	93.0 ± 0.7
Density gcm <sup>-3</sup>	8.32 ± 0.01	8.26 ± 0.01
Yield stress MPa	753.4 ± 30.7	1048.8 ± 50.9
UTS MPa	1054.5 ± 24.1	1436.9 ± 46.9
Oxidation index	16.50 ± 0.01	19.2 ± 0.01
Stress rupture MPa	599.4 ± 18.8	1137.5 ± 208.3
Resistivity μΩcm	9.02 ± 0.01	8.93 ± 0.01
Entropy Jmol <sup>-1</sup> K <sup>-1</sup>	11.60 ± 0.01	14.50 ± 0.01

	Ni	Cr	Co	Mo	Ti	Al	Ta	Hf	C	W	Mn	B	Ta	Si	Zr	Nb	Fe	T	t
RR1000	52	15	19	5	3.6	3	2	0.5	0.1									800	8
Optimal	56	17	1.0	4.0	1.5	4.3	0.2	0.1	0.2	6.0	0.1	0.1	0.2	0.1	0.2	5.6	3.4	980	61

# Optical micrograph – Ni disc alloy

Ni disc alloy

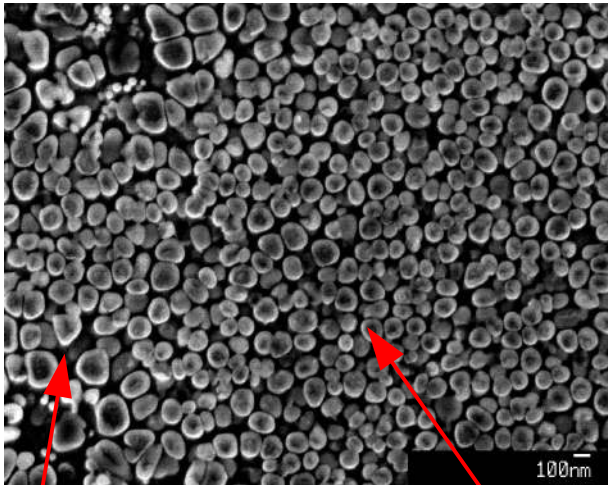


Y

Y'

# Optical micrograph – Ni disc alloy

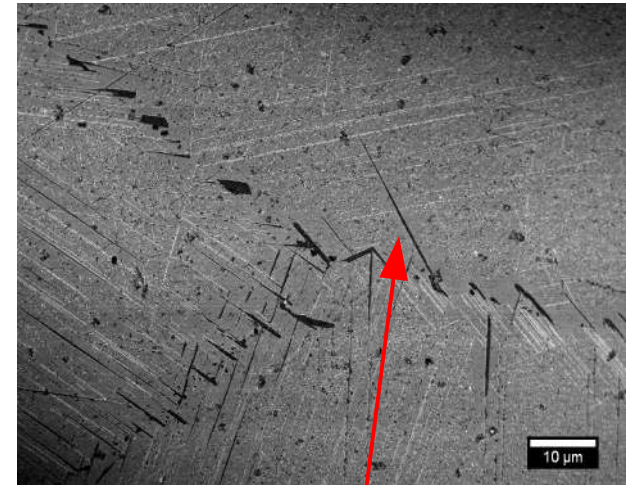
Ni disc alloy



$\gamma$

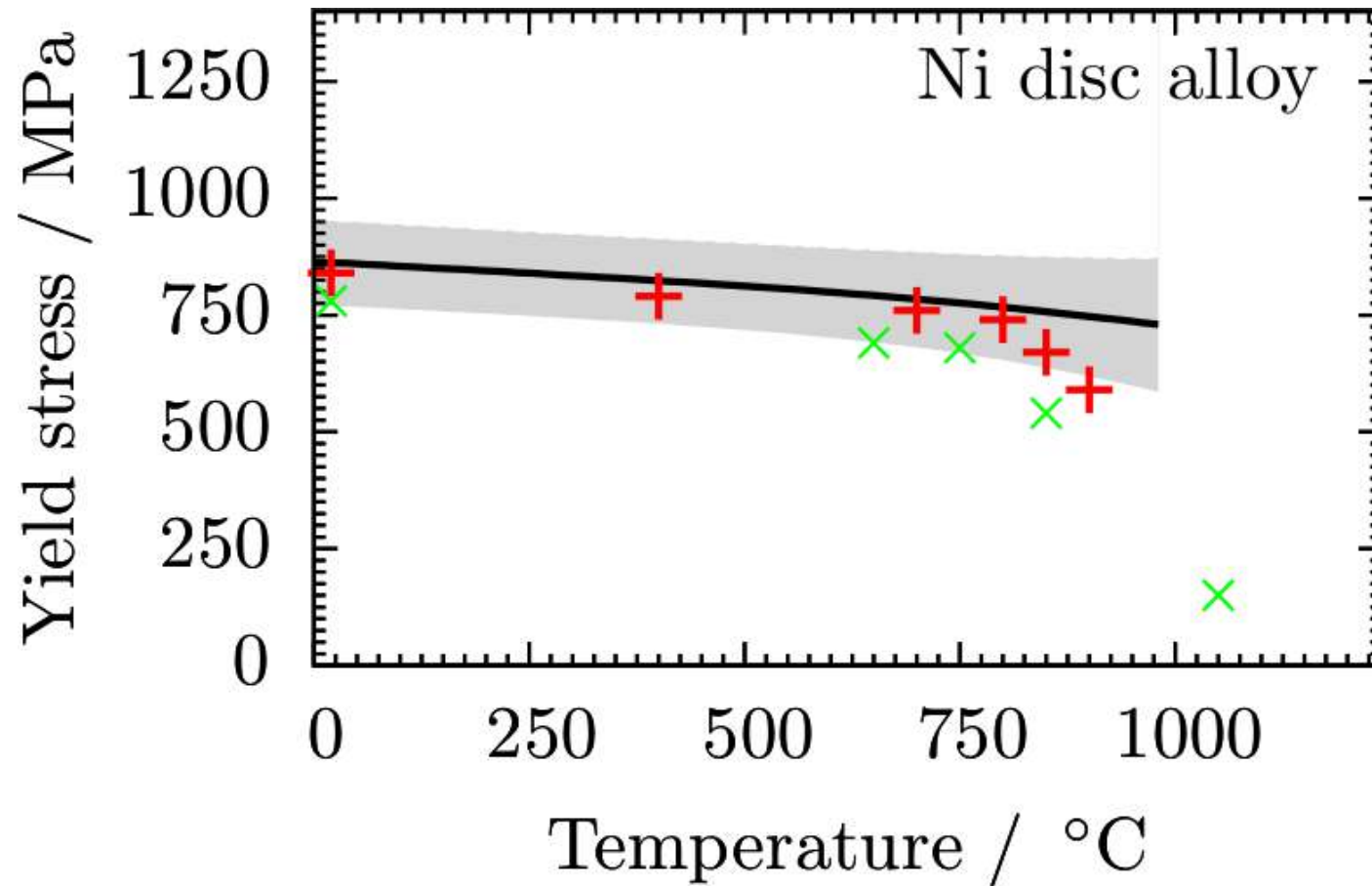
$\gamma'$

Ni alloy with  $\eta$  phase



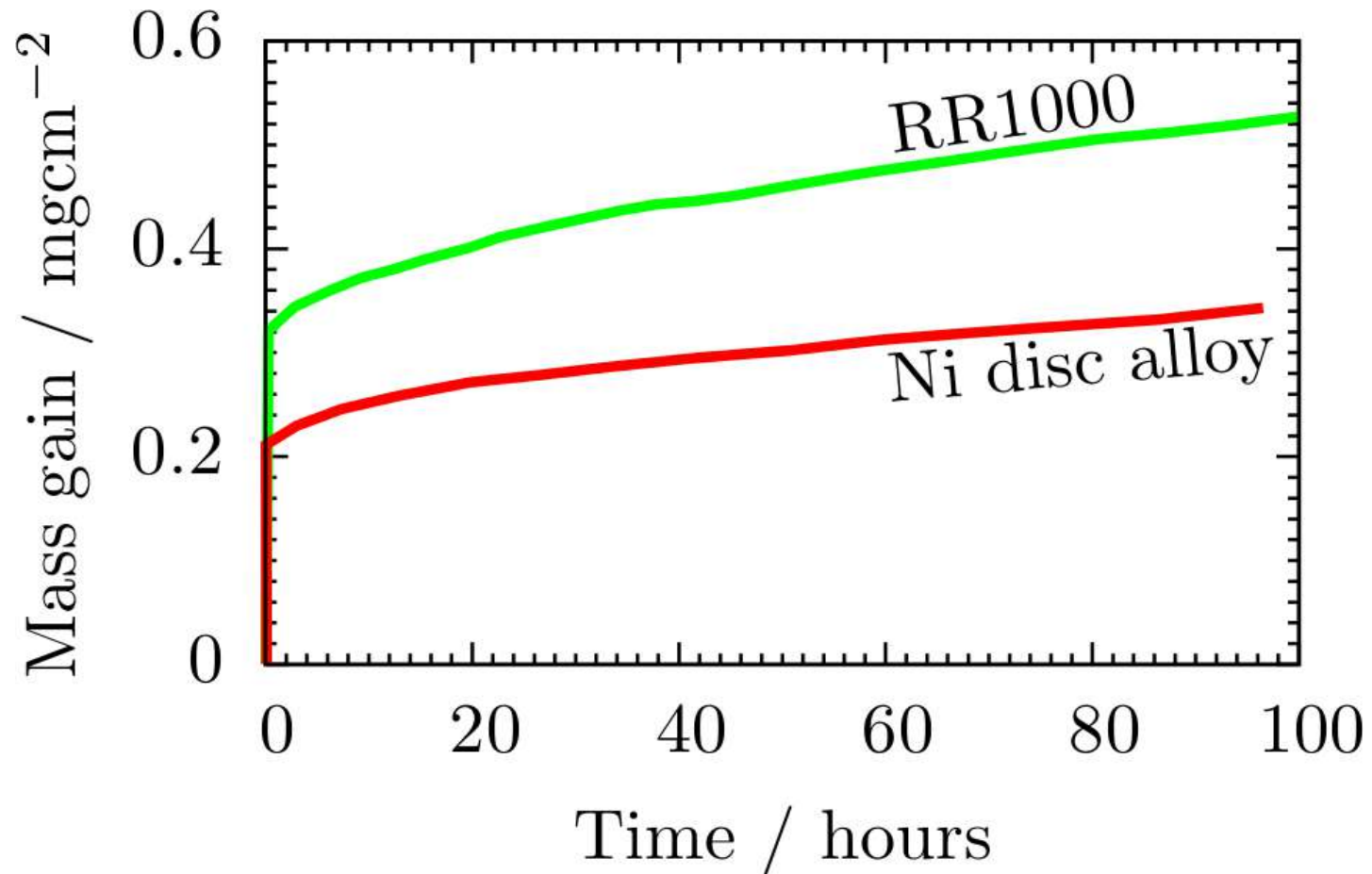
$\eta$

# Yield stress

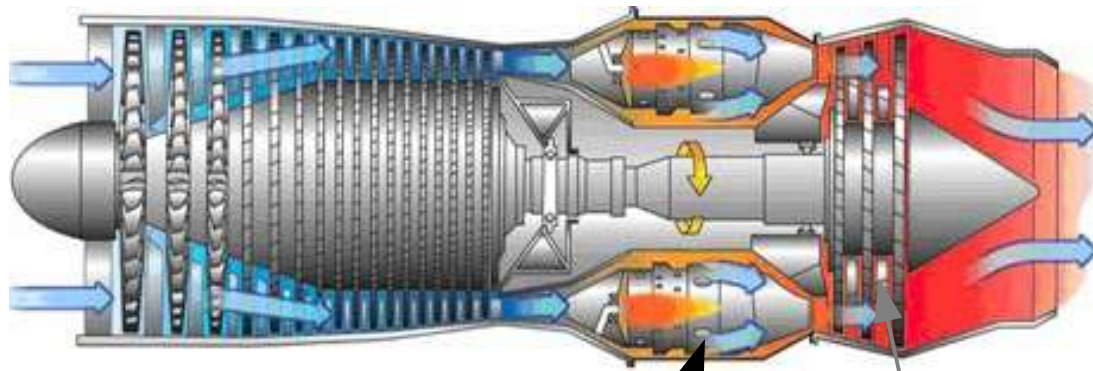




# Oxidation



# Predicted alloys



**Combustor  
liner**

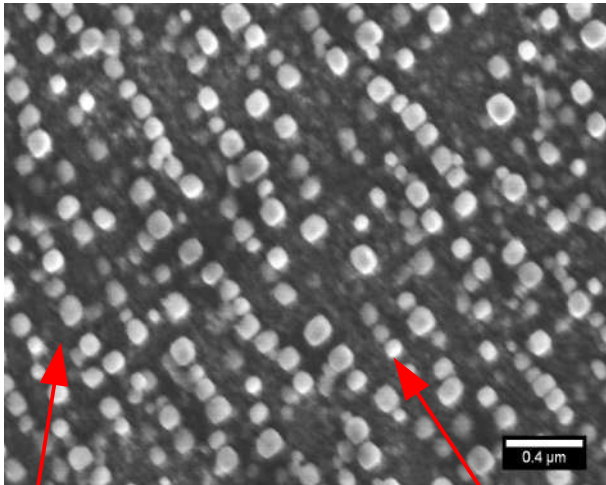
**2x disc  
alloy**



**2x forging  
hammer**

# Optical micrograph – Ni combustor liner

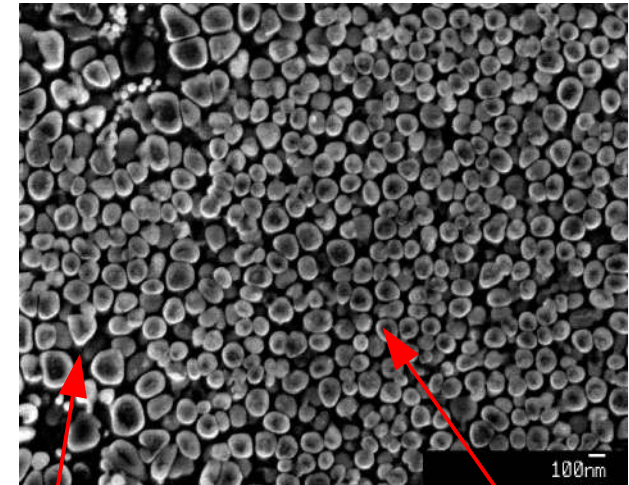
Ni combustor liner



$\gamma$

$\gamma'$

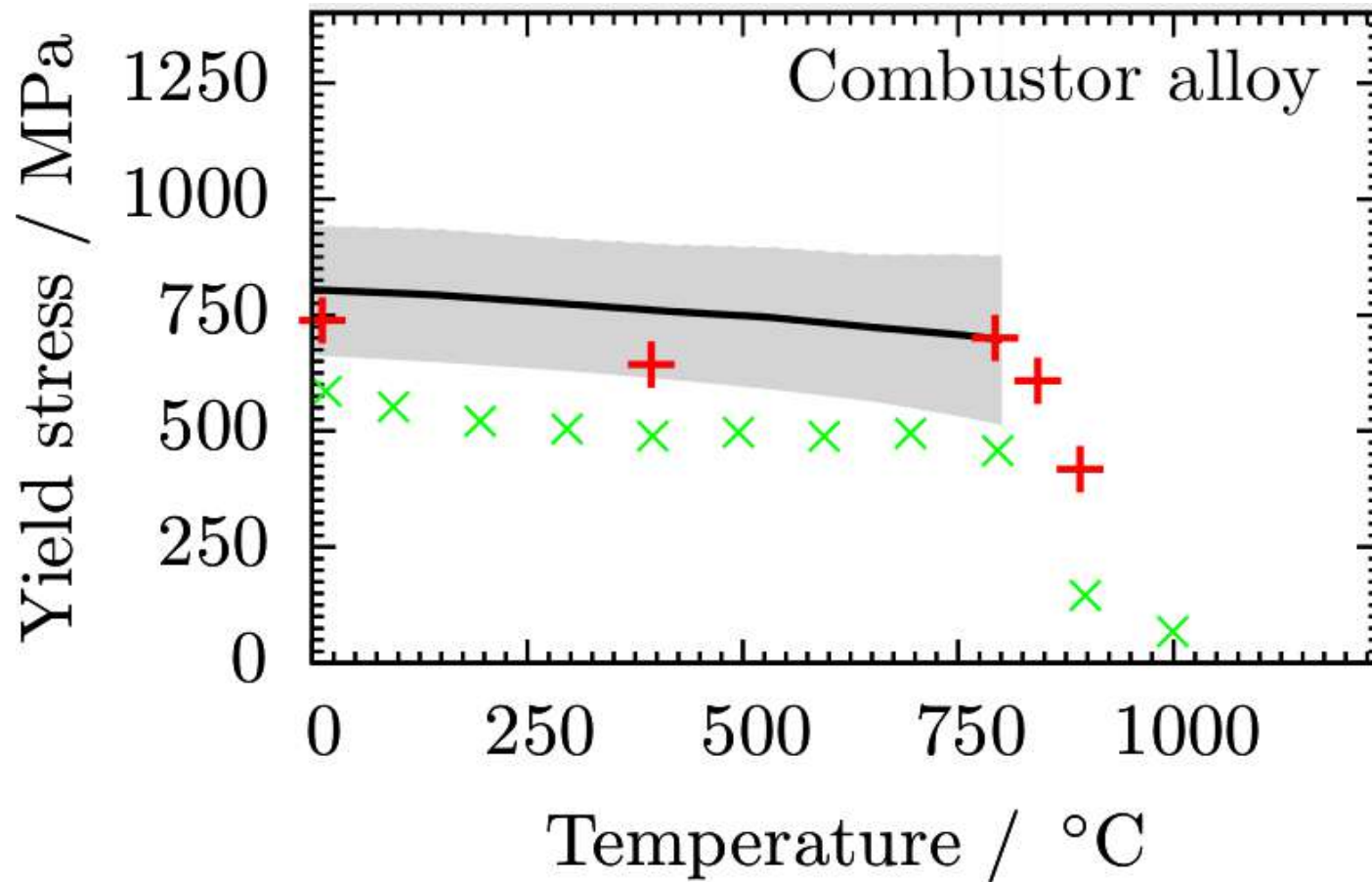
Ni disc alloy



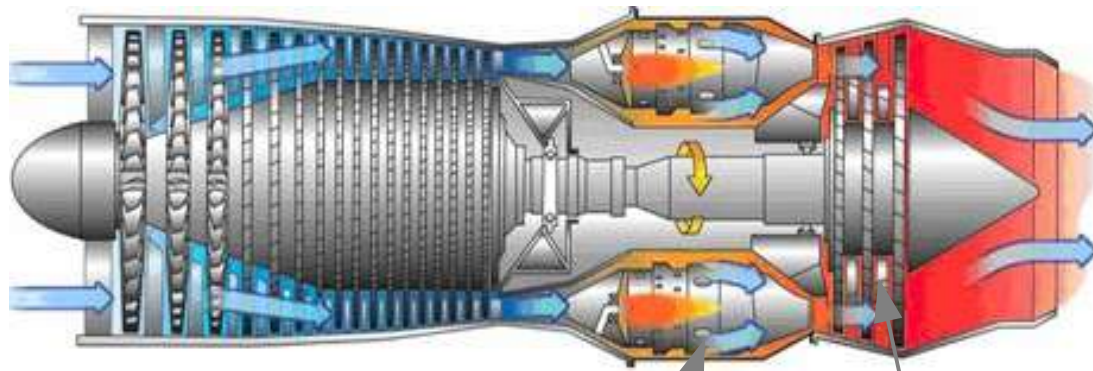
$\gamma$

$\gamma'$

# Yield stress



# Predicted alloys



Combustor  
liner

2x disc  
alloy



2x forging  
hammer

# Case study: TZM

<b>At 1000°C</b>	<b>TZM</b>
<b>Cost \$lb<sup>-1</sup></b>	13.46 ± 0.01
<b>UTS MPa</b>	1054.5 ± 24.1

	<b>Mo</b>	<b>Ti</b>	<b>C</b>	<b>Zr</b>	<b>Hf</b>	<b>W</b>	<b>Nb</b>
<b>TZM</b>	99.4	0.5	0.02	0.08			

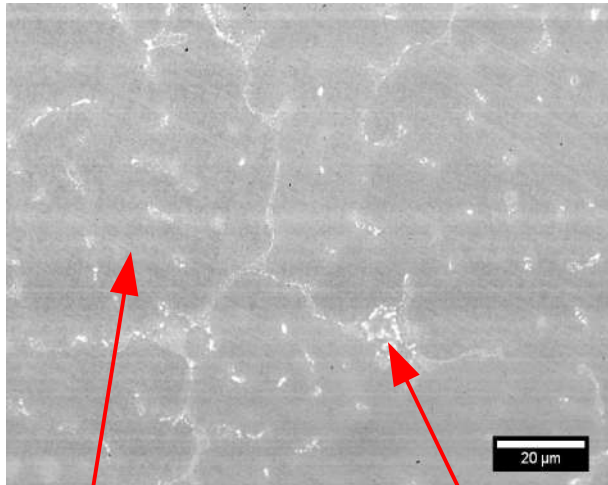
# Case study: improved

At 1000°C	TZM	Optimal
Cost \$lb <sup>-1</sup>	13.46 ± 0.01	11.67 ± 0.01
UTS MPa	42.2 ± 0.9	39.7 ± 3.1

	Mo	Ti	C	Zr	Hf	W	Nb
TZM	99.4	0.5	0.02	0.08			
Optimal	82.7	1.0	0.2	0.9	9.0	0.5	5.7

# Optical micrograph – Mo forging alloy

Mo forging alloy



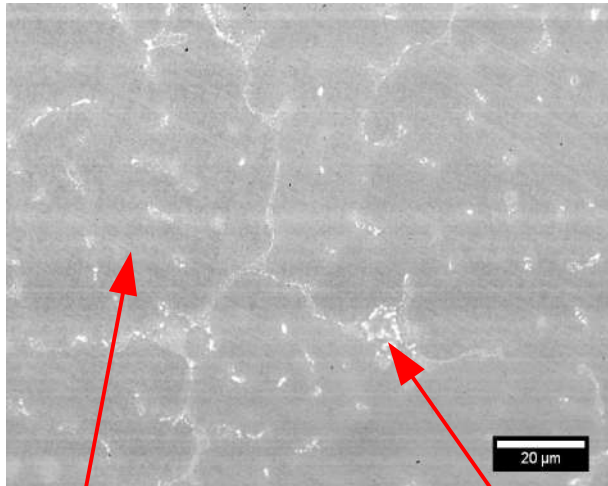
$\alpha$

HfC



# Optical micrograph – Mo forging alloy

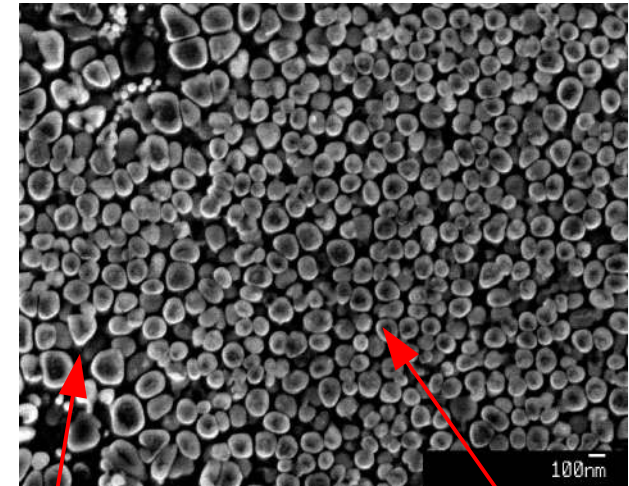
Mo forging alloy



$\alpha$

HfC

Ni disc alloy



$\gamma$

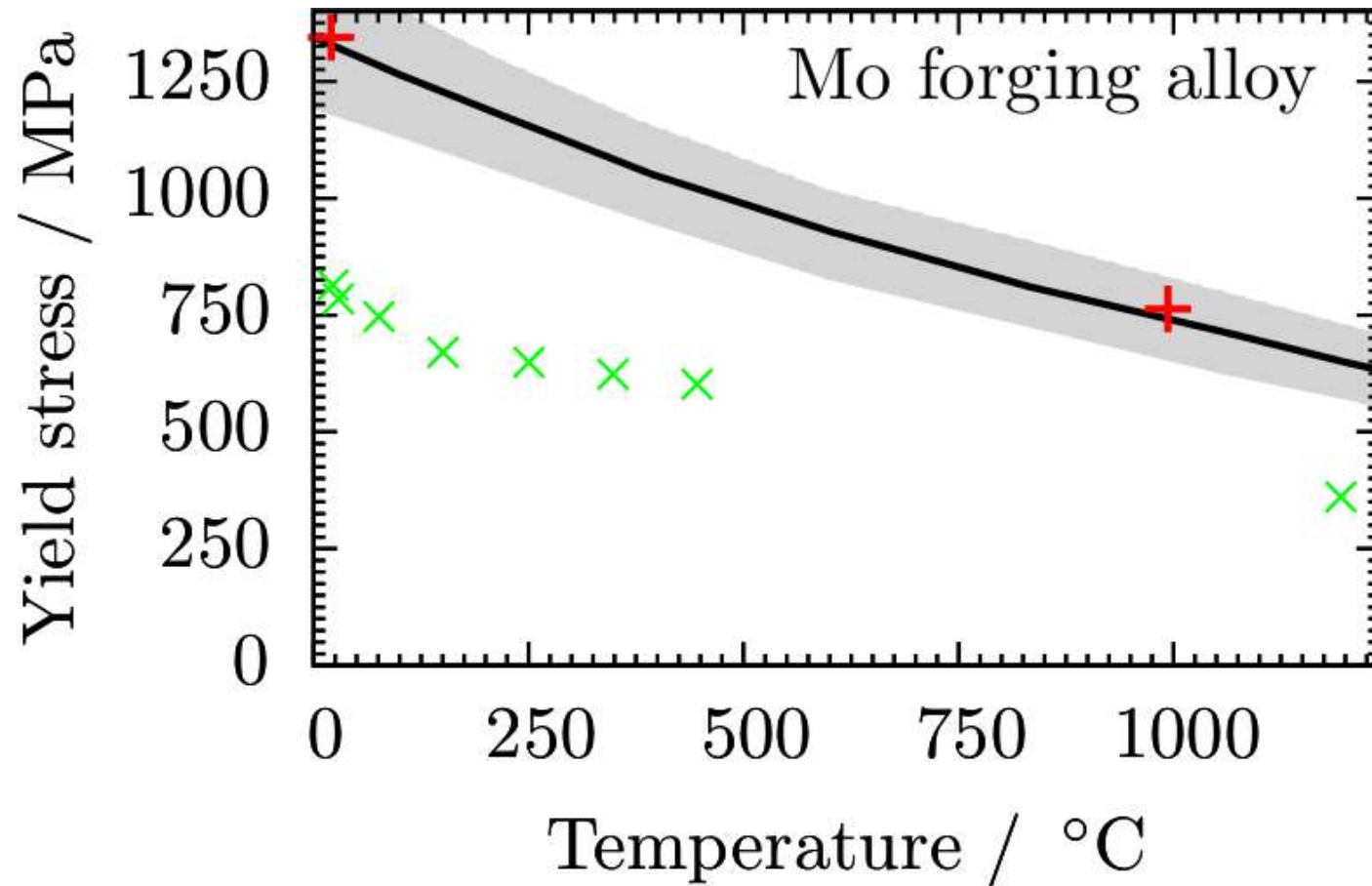
$\gamma'$

	Mo	Ti	C	Zr	Hf	W	Nb
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<b>TZM</b>	99.4	0.5	0.02	0.08			
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<b>Optimal</b>	82.7	1.0	0.2	0.9	9.0	0.5	5.7
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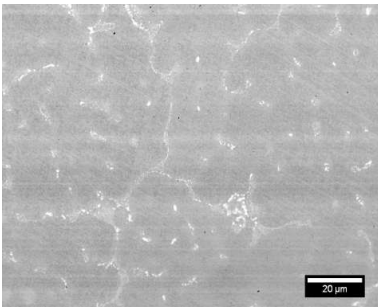
# Yield stress



# Alloys designed

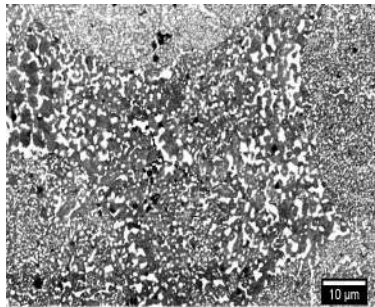
## Mo-Hf forging alloy

Patent GB1307533.8 (2013)



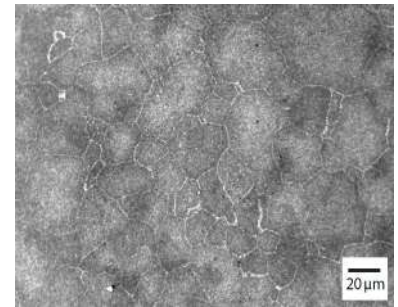
## Mo-Nb forging alloy

Rolls-Royce invention  
NC13024 (2013)



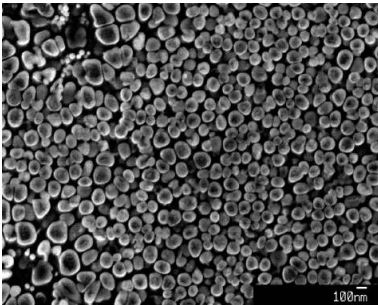
## RR1000 grain growth

Acta Materialia, **61**,  
3378 (2013)



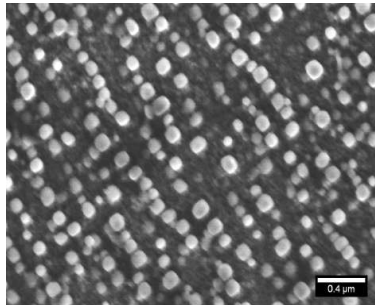
## Ni disc alloy

Rolls-Royce invention  
NC12261 (2012)



## Ni combustor liner

Rolls-Royce invention  
NC13006 (2013)



## High entropy alloy

